

**E: Hydrology Report and Water Quality
Management Plan**



PRELIMINARY HYDROLOGY REPORT

MULTI-USE DEVELOPMENT AT FORMER IRWD SITE

Lake Forest, California

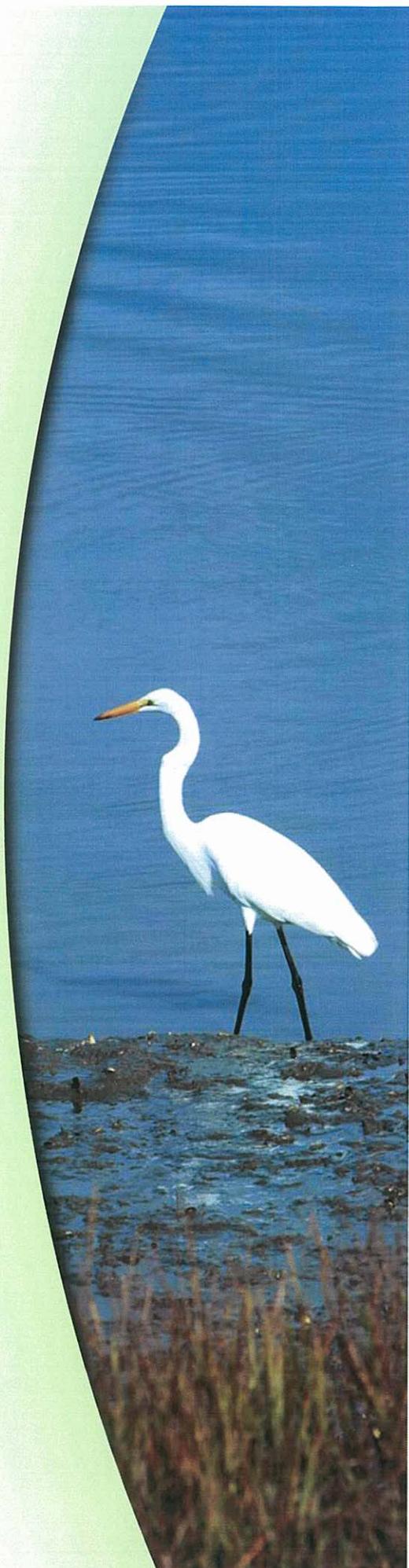
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Job Number: 658.02.01

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1.0 INTRODUCTION

1.1 GEOGRAPHIC SETTING

The Study area consists of 99 acres± and is located in the City of Lake Forest, California. It lies south of Commerce Centre Drive and is bound to the north and east by an existing commercial development, and to the south by the Baker water treatment facility. See Figure 1, Vicinity Map.

1.2 PURPOSE OF THIS REPORT

The purpose of this report is to accomplish the following objectives:

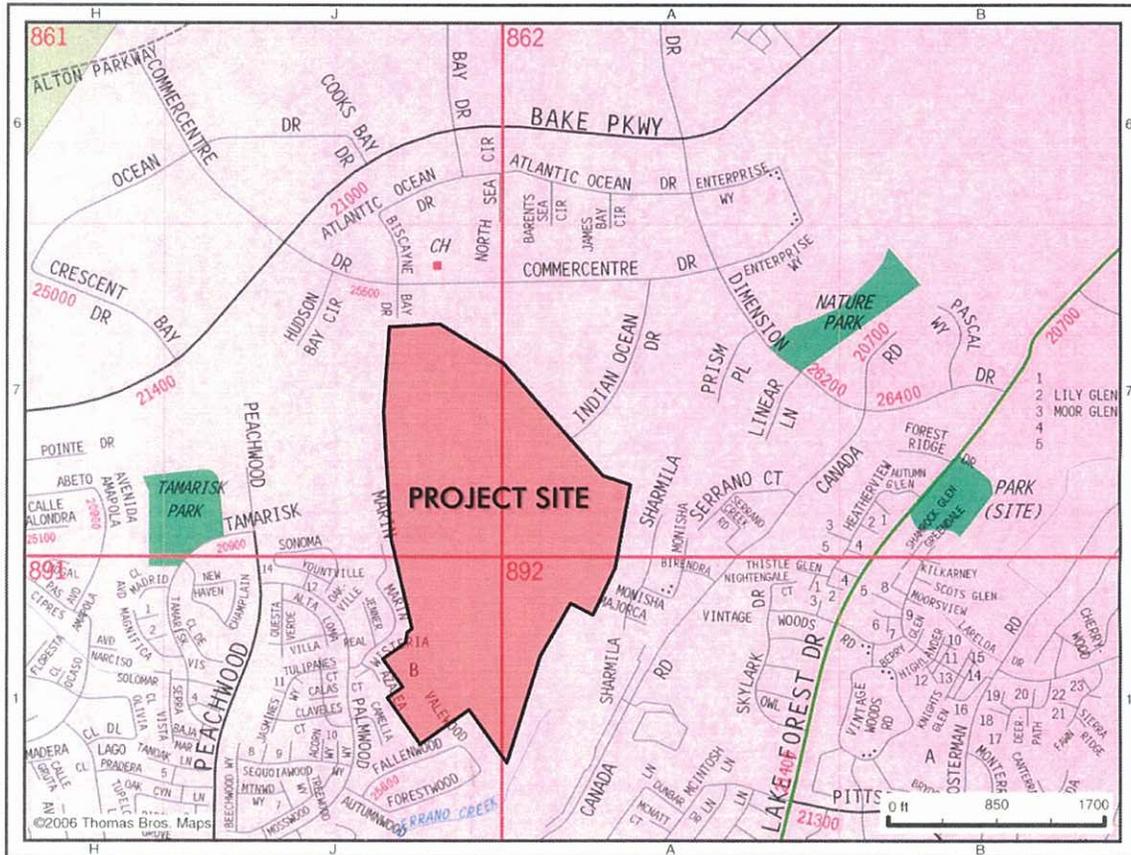
To determine the storm water discharges generated within the project under existing and proposed conditions. (see Appendices 2 and 3).

To evaluate discharges and comment on the design and make recommendations regarding the design and possible storm drain and hydrology related issues in regard to Serrano Creek.

1.3 REFERENCES

- O.C.E.M.A. Hydrology Manual
- O.C.E.M.A. Design Manual

1.4 PROJECT SITE LOCATION MAP



2.0 EXISTING TOPOGRAPHIC & HYDROLOGIC CONDITIONS

2.1 EXISTING TOPOGRAPHY

The site has been rough graded per the Los Alisos Water District (LAWD) plans "Zone 1 – Emergency Storage Reservoirs", 1989 record drawings. Los Alisos Water District has been taken over by Irvine Ranch Water District (IRWD).

The site slopes generally toward the east and Serrano Creek. The site was graded with a variety of basins, ridges and terraced slopes. Significant to the site is a deep ravine on the northeasterly portion of the property. A large portion of the development site drains to this heavily wooded and brushed tributary to Serrano Creek.

2.2 EXISTING DRAINAGE PATTERN

There is no run-on to the site from outside areas. The majority of the site currently flows easterly into Serrano Creek via three existing pipe discharge points. Three small areas also sheet flow directly to Serrano Creek. Those areas (designated OS-3, 4 & 5) are not a part of the development area and their drainage patterns will not be changed.

The current drive approach to the site from Biscayne Bay Drive (designated OS-1 & 2), sheet flows toward Biscayne Bay Drive where flow is picked up via an existing street catch basin.

Two small areas (designated OS-6 & 7), on the west side of the current IRWD buildings, flow to existing developed areas and their existing terrace drains. These areas are not part of the development area and their flow pattern will not change.

Two areas (designated OS-8 & 9), on the west side of the development site, sheet flow westerly into undeveloped land. There is a proposed tract over a portion of the undeveloped land.

2.3 EXISTING STORM DRAIN FACILITIES

Per the LAWD plans previously cited and per visual inspection of the site, there are a number of basins and attendant pipes that currently serve the site. Those basins, risers, outlets and pipes are in various states of repair. Many of the basins are overgrown with brush and several of the outlet pipes were found to be partially buried by silt build-up. There are three outlets to Serrano Creek from the site in addition to the small areas that sheet flow to the creek.

Pipe 'A' drains a large portion of the development site and drains the ravine on the northeasterly portion of the site.

Pipe 'B' drains the abandoned LAWD headquarters building site, a portion of the 'emergency storage reservoir' site and the northerly parts of the above ground tank site.

Pipe 'C' drains the southerly portion of the IRWD above ground tank site. Pipe C is not a part of the development area and is not addressed in this report.

2.4 EXISTING CONDITIONS



3.0 PROPOSED STORM DRAIN FACILITIES

Seven (7) local storm drain systems are proposed for this project as follows:

3.1 STORM DRAIN LINES "A" THROUGH "F"

This system will drain the majority of the site and flows to the proposed detention and water quality basin located adjacent to existing water tanks. Storm flow will be detained in this basin during periods of peak rainfall and released through a proposed culvert to Serrano Creek. The outlet in Serrano Creek will consist of an outlet structure with rip rap to reduce outlet velocities into the creek. The peak 100 year event discharge at this outlet is approximately 134 cfs.

3.2 STORM DRAIN LINE "G"

This system will drain the future Civic Center site adjacent to Serrano Creek. Flow will be directed to a proposed detention and water quality basin adjacent to existing outlet A before being released into Serrano Creek. The outlet of this basin will join the exist 72" pipe at outlet A. The peak 100 year event discharge at this outlet is approximately 33 cfs.

The total 100 year peak discharge from both outlets is approximately 167 cfs with detention. This is less than the existing flow of approximately 200 cfs into Serrano Creek.

4.0 HYDROLOGY STUDY

4.1 STORM FREQUENCY

For the purposes of this study, the 100-year hydrology was calculated. The existing hydrology was calculated for the two outlet points that will be affected by the development. Proposed hydrology for the rough grade state was calculated. Only a conceptual site plan was available for use in this study, therefore a proposed hydrology was calculated using the proposed uses of the various development areas using Alternative IX. No storm drain or street layouts were available, so only a very preliminary storm drain layout was used. Times of concentration could be expected to be longer in the developed condition with actual street and storm drain layouts.

In addition to the 100 year discharge the 2 year discharge under existing and proposed conditions was also calculated.

The 2 year discharge and volumes were used to evaluate the hydrologic conditions of concern to be evaluated in the Water Quality Management Plan (WQMP).

4.2 METHODOLOGY

The hydrology was prepared in conformance with the Orange County Hydrology Manual using AES software (Appendix 3).

Unit hydrographs were then developed using AES software to determine discharge volumes for the proposed condition. Hydrographs for 100 year flows were then routed through the proposed detention basins using HydroCAD modeling software (Appendix 4).

Unit hydrographs were also developed for the 2 year event using existing and proposed conditions. This analysis was done to determine the volume that may or may not need to be retained onsite as part of the new water quality requirements.

5.0 HYDRAULIC REPORT (ANALYSIS OF THE MAIN LINE STORM DRAIN)

Hydraulic analysis of mainline storm drains will be determined during final plan preparation of the project site.

6.0 DESIGN CRITERIA

The proposed storm drain systems will be designed so as to be consistent with the following goals and guidelines:

- A. All buildings shall be protected from flooding during a 100-year frequency storm.
- B.
 1. Onsite design storm is based on a 25-year frequency. In sump conditions for catch basins and the connecting storm drains also use a 25-year frequency.
 2. Offsite design storm frequency, subject to individual review by the City, should be in accordance with the O.C.E.M.A. Hydrology Manual.
- C.
 1. Velocity should not exceed 20 FPS in a standard wall R.C.P.
 2. Where velocity exceeds 20 FPS, a special wall R.C.P. with a minimum of 1½-inch steel clearance on the inside surface shall be used.
 3. Maximum velocity in special cover R.C.P. shall be 45 FPS.
- D. On arterial highways, one (1) 12' lane each direction should be clear of water, with a 10-year storm. In sump conditions, a 25-year storm event shall be used.
- E. On local streets, flow should not exceed top of curb, for a 10-year storm event, and in sump conditions, a 25-year storm event shall be used.

Cross gutter is not allowed at any through street.

- F. Catch basins are to be constructed at all four corners of arterial highway intersections.
- G. Open cut is not allowed at any existing arterial highway. Pipe must be jacked across street.
- H. Maximum W.S. in CB's for design conditions shall be 0.5' below inlet (FL.) elevation.
- I. Once water is picked up in a storm drain, it should remain in the system.
- J. Pipe size may not be decreased downstream without the City's approval.
- K. Branching of flow is not allowed.
- L. Provide hydraulic and energy grade line calculations and plot of hydraulic grade line on plans with table of appropriate hydraulic data.
- M. The ratio of normal velocity to critical velocity should be less than 0.9 or greater than 1.2.

- N. All pipes and conduits laid parallel to the roadway shall be placed at least 30" below the roadway surface. However, when pipe depth is in excess of 10' (measured from top of pipe to ground surface), the City's approval is required prior to the initial design of the system.
- O. Junction structures should be designed according to the O.C.F.C.D. "Design Manual" or utilize City of Orange Standard Plans.
- P. Storm Drain Easement width shall be determined in the following manner:
1. $D = 36''$ or smaller – Distance from top of pipe to ground level times 1.5 + diameter of pipe + 2.0' (When cover exceeds 10', use 2 below.)
 2. $D = 39''$ or greater – a. Distance from bottom of pipe to ground level times 2.0 + diameter of pipe + 2.0'.

In any case, the width of easement shall not be less than 10.0' in width.

- Q. Easement shall be exclusively for storm drain purposes.
- R. Storm drain with high fills:

1. Fill Greater than 40 Feet

Storm drains which are installed with cover greater than 40 feet shall have a diameter a minimum of 12 inches larger than that required for hydraulic adequacy and shall be constructed using pre-stressed concrete pipe.*

2. Fill between 30 and 40 Feet

Storm drains which are installed with cover between 30 and 40 feet shall have a diameter a minimum of 12 inches larger than that required for hydraulic adequacy and shall be constructed using pre-stressed concrete pipe if the subgrade of the pipe is in a fill area.* If subgrade is in native soil, reinforced concrete pipe may be used.

3. Fill Between 20 and 30 Feet

Storm drains which are installed with cover between 20 and 30 feet shall be constructed using reinforced concrete pipe. A pipe diameter greater than that required for hydraulic adequacy may be required if, in the opinion of the City Engineer's staff, the particular conditions involved warrant the larger size.

4. Fill Less Than 20 Feet

Normal criteria for storm drain design shall be followed.

* Exceptions may be made for a roadway crossing of a natural watercourse which will remain undisturbed with future development.

7.0 RESULTS AND CONCLUSIONS

At outlet A to Serrano Creek the 100 year peak discharge is approximately 33 cfs. This is 112 cfs less than the existing condition due to site configuration and detention See Exhibit A on next page.

At outlet B to Serrano Creek the 100 year peak discharge is approximately 133 cfs after detention. This is approximately 78 cfs more than the existing condition.

Overall, flows discharged to Serrano Creek is approximately 33 cfs less than the existing condition. The reach of the creek upstream of outlet B will have flow reduced by approximately 112 cfs during the 100 year event. This will greatly reduce the potential for erosion in this reach. Downstream of outlet B the reduced total flow also reduces the potential for erosion, upstream of outlet A the flow in the creek is not affected by the project. This includes the reach of the creek adjacent to homes on Sharmillo Drive. The table below summarizes these discharges to each existing outlet to Serrano Creek.

Existing Outlet	Exist. Q ₁₀₀	Prop Q ₁₀₀
A	145 cfs	33 cfs
B	55 cfs	134 cfs
TOTAL	200 cfs	167 cfs +/-

Under the 2 year event no more than 105% of the pre development volume and peak flow will be allowed to flow off site. This may be accomplished in a variety of ways which is discussed in more detail within the WQMP. Shown below is a table summarizing the 2 year event conditions.

Summary of 2 Year Event Conditions

Outlet A

Sub Area	Area (ac)	Existing Conditon			Proposed Condition			
		Q (cfs)	TC (min)	Vol (ac-ft)	Area (ac)	Q (cfs)	TC (min)	Vol (ac-ft)
Area A Civic Center Direct to Creek	59.6	38.38	20.96	4.02	12.4 2.95	20.54 1.3	6.63 25.39	
Totals	59.6	38.38	20.96	4.02	15.35	21.84	6.63	1.63

Outlet B

Sub Area	Area (ac)	Existing Conditon			Proposed Condition			
		Q (cfs)	TC (min)	Vol (ac-ft)	Area (ac)	Q (cfs)	TC (min)	Vol (ac-ft)
Area B Area A Tank Site	15.4	17.61	8.95	0.98	63.4 3.83	73.06 3.46	8.36 13.07	
Totals	15.4	17.61	8.95	0.98	67.23	76.52	8.36	6.69

Project Totals

	Area (ac)	Existing Conditon			Proposed Condition			
		Q (cfs)	TC (min)	Vol (ac-ft)	Area (ac)	Q (cfs)	TC (min)	Vol (ac-ft)
Difference In Area Is Due To Areas OS-8 & OS-9	75	55.99		5.0	82.58	98.36		8.32

5% of existing condition volume = 0.25 ac-ft

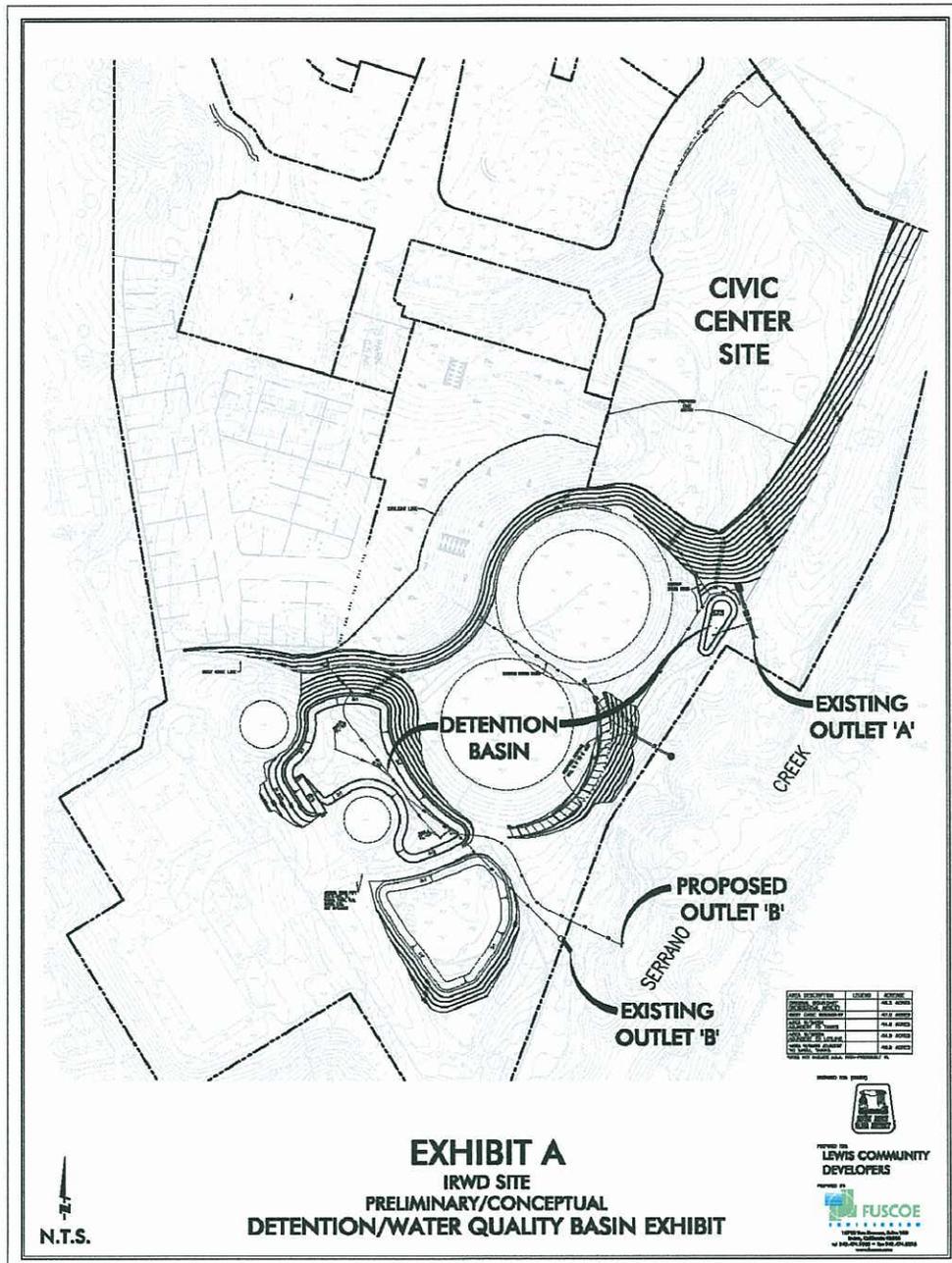
Therefore acceptable total volume = 5.25 ac-ft

Proposed condition total volume = 8.32 ac-ft

Therefore total volume to be retained onsite = $8.32 - 5.25 = 3.07$ ac-ft

As shown in the table the total additional volume due to development is approximately 3.3 ac-ft. Additional discussion of retention alternatives is presented in the WQMP for the project.

7.1 DETENTION/WATER QUALITY BASIN – EXHIBIT A



8.0 APPENDICES

<i>Appendix 1</i>	<i>Storm Water Protection Goals</i>
<i>Appendix 2</i>	<i>Preliminary 100-Year Existing Hydrology</i>
<i>Appendix 3</i>	<i>Preliminary 100 year Proposed Hydrology</i>
<i>Appendix 4</i>	<i>Detention Calculations</i>
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CHAPTER 1

DESIGN CRITERIA

The following design criteria shall be used for storm drain and local drainage structures built for dedication to the County of Orange, Orange County Flood Control District, or for private facilities within unincorporated Orange County.

Regional or Sub-Regional design storm frequencies are subject to individual review by the Agency and should be in accordance with the 1986 Hydrology Manual and Flood Protection Goals. This manual does not supersede any information contained within the Orange County Drainage Area Management Plan (DAMP), and is intended to be consistent with the DAMP.

I. PROTECTION LEVELS

A. Structures

The goal is to provide 100-year protection for all habitable structures pursuant to Public Services and Facilities Element of the General Plan.

B. Streets

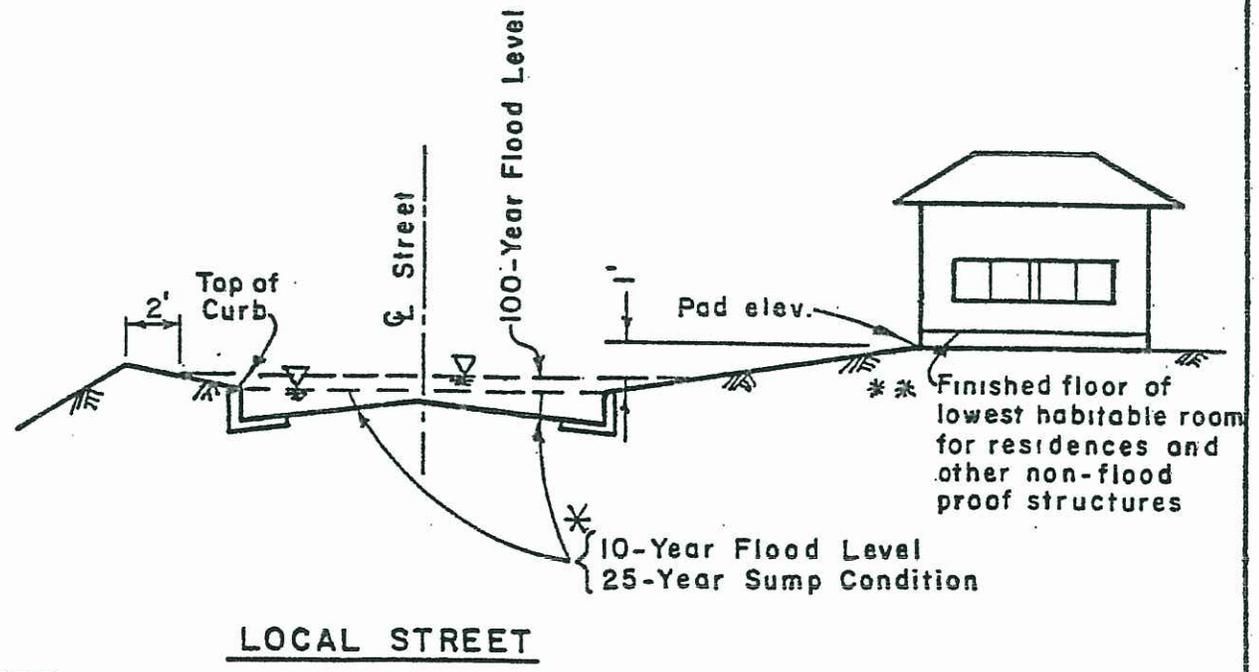
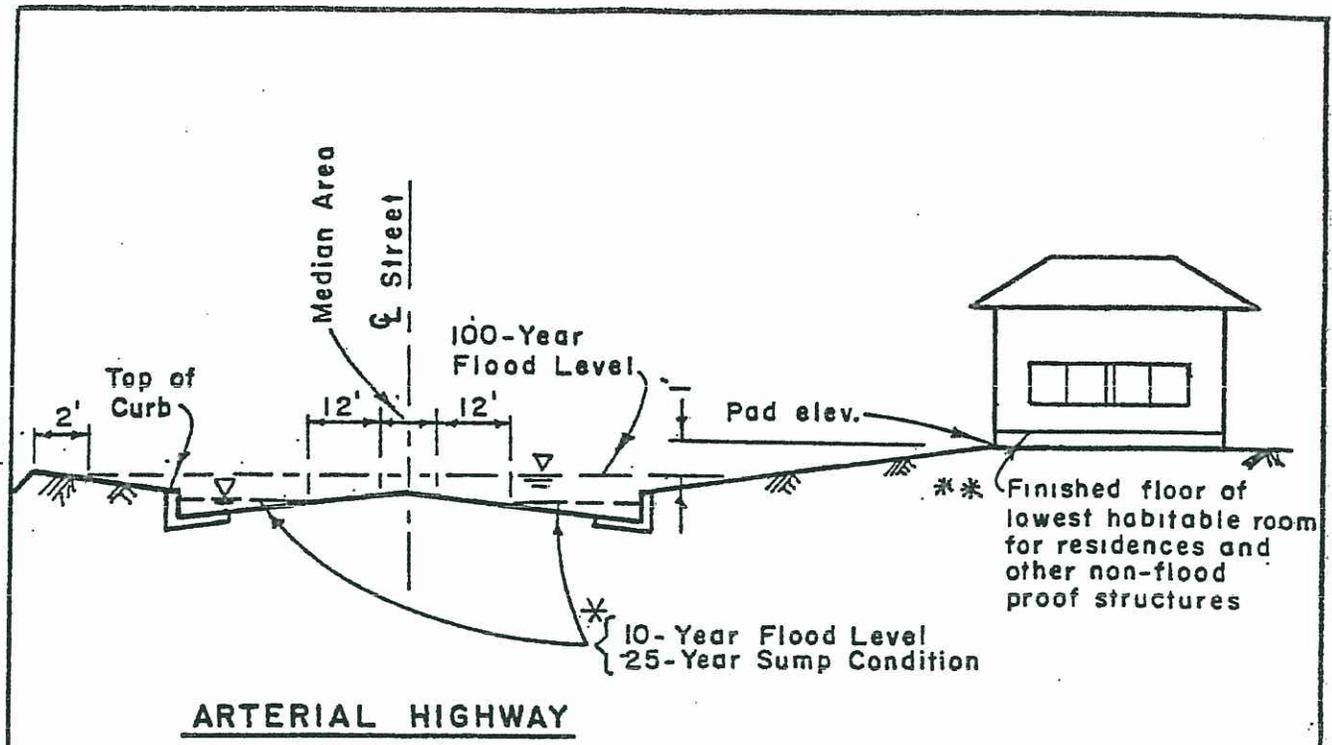
Street criteria for 100-year storm flow is shown on the attached Figure 1-1, Flood Protection Goals.

1. Arterial Highway

- a. One travel lane (use 12 foot if not determined) shall be free from inundation in each direction in a 10-year storm.
- b. In a sump condition, one travel lane (use 12 foot if not determined) shall be free from inundation in each direction in a 25-year storm.
- c. Median and left-turn pockets shall not be considered as a travel lane.
- d. In places where superelevation occurs on arterial highways an inlet shall be provided as necessary to preclude drainage across the travel lanes. The catch basin shall intercept a minimum of a 10-year storm. Local depressions are not to be used for inlets at medians; grate opening or side opening/grate combination (for which future paving overlap will not create a drop) are recommended. Flooding width from median curbs in superelevated sections shall not exceed two feet.

C. General Criteria

1. Storm drains with tributary areas of less than 640 acres are to be designed for a minimum of 10-year frequency below top of curb



NOTE

*For Arterial Hwy and Local Street, depth times velocity cannot exceed six

** The elevation of the lowest floor of buildings, including basements or cellars, must be at least 1 foot above the 100-year flood water surface elevation pursuant to Section 7-9-113.5 of the County Ordinance.

ORANGE COUNTY E.M.A.		
FLOOD PROTECTION GOALS		
1986	1 OF 1	

using a combination of street and storm drain flow. In sump conditions, catch basins and the connecting storm drains should be designed to a 25-year frequency.

2. Regional or Sub-Regional design storm frequency are subject to individual review by the Agency and should be in accordance with the 1986 Hydrology Manual and Flood Protection Goals and must be designed to contain, as a minimum, the Federal Emergency Management Agency's (FEMA) 100-year discharges used for defining Flood Insurance Rate Map floodplains.
3. The product of the depth of water, y (ft.) at the curb times velocity, v (fps), shall not exceed six for any street. This criteria applies to storms up to a 25-year frequency.
4. Leveed channels are generally prohibited for local drainage applications. The use of leveed channels or floodwalls* in local drainage situations shall include appropriate justification.

II. FREEBOARD

A. Purpose

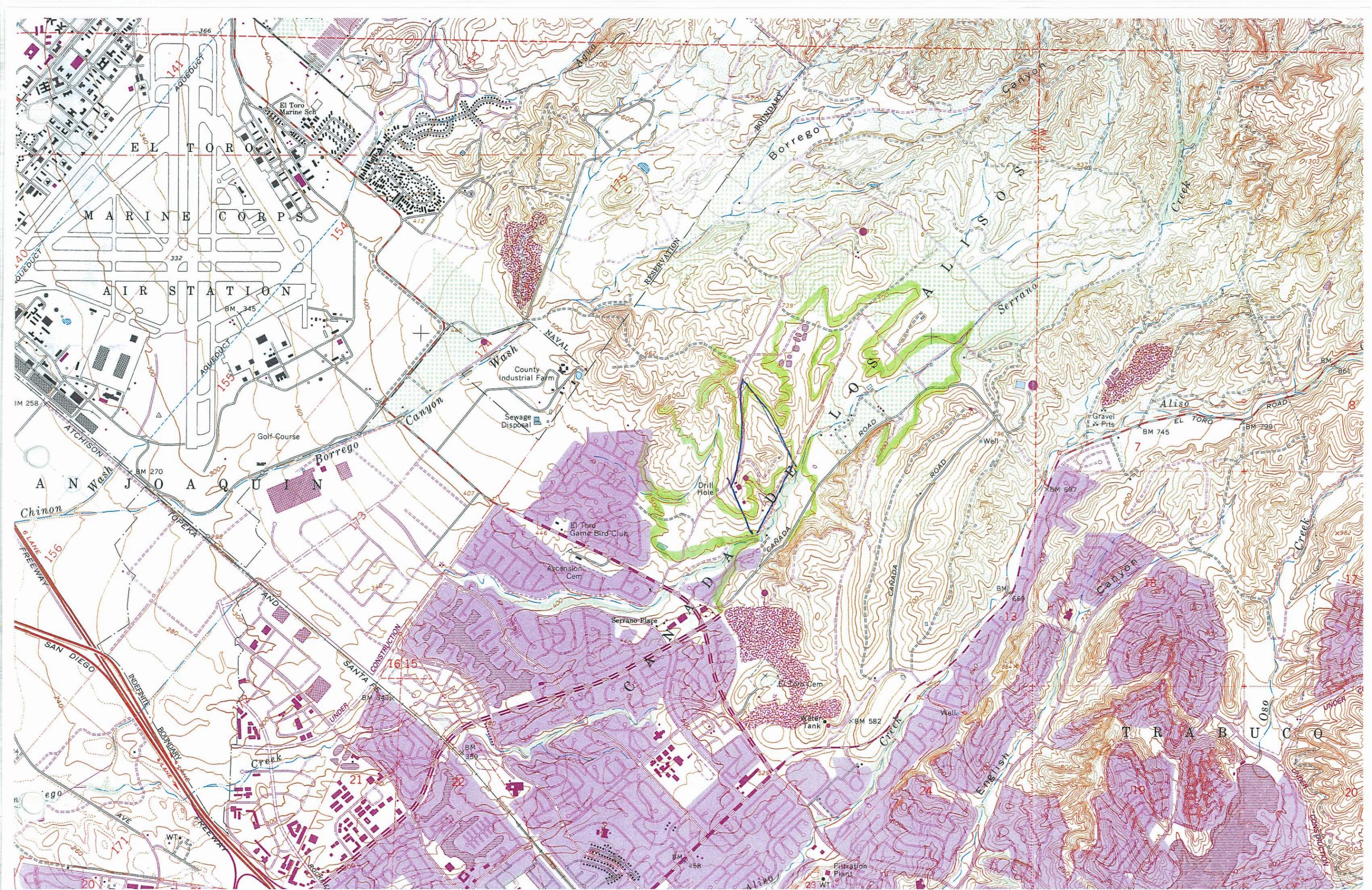
Freeboard is provided to insure that the desired degree of protection will not be reduced by unaccounted factors which may affect channel hydraulics but which are not required to be specifically analyzed in design. These factors include, but are not limited to, variations in Manning's "n" due to channel bottom conditions, uncertainties in the selection of Manning's "n", variation in stage-discharge relationships, variation in velocity from average velocity, sedimentation, debris, bulking, and air entertainment. When any of the above factors are expected to be significant, its effect shall be separately estimated and necessary provisions included in design to account for same.

B. Reference Elevations

Freeboard is the vertical distance from the design hydraulic grade line as defined below and as shown in Figure 1-2.

1. Top of levee in ultimate unlined earth levee channels.
2. Top of rock where riprap slope protection is utilized.
3. Top of wall or structural section in concrete channels.
4. Soffit where box-conduits or culverts are designed as open channels.

*A floodwall is a wall, in lieu of a levee, which projects above the surrounding ground for the purpose of conveying flood waters. See summary of FEMA's National Flood Insurance Program regulations § 65.10.44 CFR (revised October 1, 1993) in Appendix 2. Engineers designing flood control levees should refer to FEMA's latest regulations before commencing design.





EXISTING AREA A

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
(c) Copyright 1983-2007 Advanced Engineering Software (aes)
Ver. 13.5 Release Date: 02/06/2007 License ID 1355

Analysis prepared by:

Fusco Engineering, Inc
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***** DESCRIPTION OF STUDY *****
* IRWD SITE - AREA A *
* 100 YEAR EXISTING HYDROLOGY *
* 6/9/08 JEL *

FILE NAME: IRWD00A.DAT
TIME/DATE OF STUDY: 10:37 06/09/2008

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USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 8.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.85
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF-WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT- / PARK-SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER WIDTH (FT)	GEOMETRIES: LIP (FT)	MANNING HIKE (FT)	FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150
2	14.0	9.0	0.020/0.020/0.050	0.33	2.00	0.0313	0.100	0.0140

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.33 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 10.00 TO NODE 11.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 252.00
ELEVATION DATA: UPSTREAM(FEET) = 706.50 DOWNSTREAM(FEET) = 688.30

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.109
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.690
SUBAREA Tc AND LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc

LAND USE	GROUP	(ACRES)	(INCH/HR)	(DECIMAL)	CN	(MIN.)
NATURAL POOR COVER						
"GRASS"	C	0.55	0.25	1.000	97	8.11
NATURAL POOR COVER						
"GRASS"	B	0.22	0.30	1.000	93	8.11
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.26						
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000						
SUBAREA RUNOFF(CFS) = 3.07						
TOTAL AREA(ACRES) = 0.77 PEAK FLOW RATE(CFS) = 3.07						

FLOW PROCESS FROM NODE 11.00 TO NODE 12.00 IS CODE = 91

>>>>COMPUTE "V" GUTTER FLOW TRAVEL TIME THRU SUBAREA<<<<<

```

=====
UPSTREAM NODE ELEVATION(FEET) = 688.30
DOWNSTREAM NODE ELEVATION(FEET) = 658.40
CHANNEL LENGTH THRU SUBAREA(FEET) = 1247.00
"V" GUTTER WIDTH(FEET) = 5.00 GUTTER HIKE(FEET) = 0.050
PAVEMENT LIP(FEET) = 0.010 MANNING'S N = .0500
PAVEMENT CROSSFALL(DECIMAL NOTATION) = 0.07000
MAXIMUM DEPTH(FEET) = 3.00
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.257
SUBAREA LOSS RATE DATA(AMC III):
  DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp        Ap        SCS
  LAND USE              GROUP   (ACRES)  (INCH/HR) (DECIMAL) CN
NATURAL POOR COVER
"GRASS"                  B        9.28     0.30     1.000    93
NATURAL POOR COVER
"GRASS"                  C       18.28     0.25     1.000    97
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.27
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 34.36
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.88
AVERAGE FLOW DEPTH(FEET) = 0.81 FLOOD WIDTH(FEET) = 26.39
"V" GUTTER FLOW TRAVEL TIME(MIN.) = 7.21 Tc(MIN.) = 15.32
SUBAREA AREA(ACRES) = 27.56 SUBAREA RUNOFF(CFS) = 74.17
EFFECTIVE AREA(ACRES) = 28.33 AREA-AVERAGED Fm(INCH/HR) = 0.27
AREA-AVERAGED Fp(INCH/HR) = 0.27 AREA-AVERAGED Ap = 1.00
TOTAL AREA(ACRES) = 28.3 PEAK FLOW RATE(CFS) = 76.24

```

END OF SUBAREA "V" GUTTER HYDRAULICS:

DEPTH(FEET) = 1.13 FLOOD WIDTH(FEET) = 35.50
FLOW VELOCITY(FEET/SEC.) = 3.50 DEPTH*VELOCITY(FT*FT/SEC) = 3.95
LONGEST FLOWPATH FROM NODE 10.00 TO NODE 12.00 = 1499.00 FEET.

FLOW PROCESS FROM NODE 12.00 TO NODE 13.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

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=====
ELEVATION DATA: UPSTREAM(FEET) = 643.00 DOWNSTREAM(FEET) = 636.00
FLOW LENGTH(FEET) = 106.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 30.0 INCH PIPE IS 20.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 21.92
ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 76.24
PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 15.40
LONGEST FLOWPATH FROM NODE 10.00 TO NODE 13.00 = 1605.00 FEET.

```

FLOW PROCESS FROM NODE 30.00 TO NODE 13.00 IS CODE = 82

>>>>ADD SUBAREA RUNOFF TO MAINLINE, AT MAINLINE Tc,<<<<<
>>>>(AND COMPUTE INITIAL SUBAREA RUNOFF)<<<<<

INITIAL SUBAREA FLOW-LENGTH (FEET) = 753.00
ELEVATION DATA: UPSTREAM (FEET) = 697.80 DOWNSTREAM (FEET) = 640.40

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 16.715

* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 3.099

SUBAREA Tc AND LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
NATURAL FAIR COVER						
"CHAPARRAL, NARROWLEAF"	B	0.63	0.30	1.000	89	16.71
NATURAL FAIR COVER						
"CHAPARRAL, NARROWLEAF"	C	3.06	0.25	1.000	95	16.71

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.26
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
SUBAREA AREA (ACRES) = 3.69 INITIAL SUBAREA RUNOFF (CFS) = 9.43

** ADD SUBAREA RUNOFF TO MAINLINE AT MAINLINE Tc:

MAINLINE Tc (MIN.) = 15.40

* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 3.247

SUBAREA AREA (ACRES) = 3.69 SUBAREA RUNOFF (CFS) = 9.93

EFFECTIVE AREA (ACRES) = 32.02 AREA-AVERAGED Fm (INCH/HR) = 0.27

AREA-AVERAGED Fp (INCH/HR) = 0.27 AREA-AVERAGED Ap = 1.00

TOTAL AREA (ACRES) = 32.0 PEAK FLOW RATE (CFS) = 85.92

FLOW PROCESS FROM NODE 13.00 TO NODE 13.50 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM (FEET) = 636.00 DOWNSTREAM (FEET) = 615.00

FLOW LENGTH (FEET) = 143.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 27.0 INCH PIPE IS 18.0 INCHES

PIPE-FLOW VELOCITY (FEET/SEC.) = 30.47

ESTIMATED PIPE DIAMETER (INCH) = 27.00 NUMBER OF PIPES = 1

PIPE-FLOW (CFS) = 85.92

PIPE TRAVEL TIME (MIN.) = 0.08 Tc (MIN.) = 15.48

LONGEST FLOWPATH FROM NODE 10.00 TO NODE 13.50 = 1748.00 FEET.

FLOW PROCESS FROM NODE 13.50 TO NODE 14.00 IS CODE = 91

>>>>COMPUTE "V" GUTTER FLOW TRAVEL TIME THRU SUBAREA<<<<<

UPSTREAM NODE ELEVATION (FEET) = 615.00

DOWNSTREAM NODE ELEVATION (FEET) = 596.00

CHANNEL LENGTH THRU SUBAREA (FEET) = 194.00

"V" GUTTER WIDTH (FEET) = 5.00 GUTTER HIKE (FEET) = 0.050

PAVEMENT LIP (FEET) = 0.010 MANNING'S N = .0150

PAVEMENT CROSSFALL (DECIMAL NOTATION) = 0.12500

MAXIMUM DEPTH (FEET) = 3.00

* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 3.216

SUBAREA LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL FAIR COVER					
"CHAPARRAL, NARROWLEAF"	A	0.53	0.40	1.000	75
NATURAL FAIR COVER					

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"CHAPARRAL,NARROWLEAF"   B       1.63    0.30    1.000    89
NATURAL FAIR COVER
"CHAPARRAL,NARROWLEAF"   C       0.03    0.25    1.000    95
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.32
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 88.77
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 17.41
AVERAGE FLOW DEPTH(FEET) = 0.59 FLOOD WIDTH(FEET) = 13.51
"V" GUTTER FLOW TRAVEL TIME(MIN.) = 0.19 Tc(MIN.) = 15.67
SUBAREA AREA(ACRES) = 2.19 SUBAREA RUNOFF(CFS) = 5.70
EFFECTIVE AREA(ACRES) = 34.21 AREA-AVERAGED Fm(INCH/HR) = 0.27
AREA-AVERAGED Fp(INCH/HR) = 0.27 AREA-AVERAGED Ap = 1.00
TOTAL AREA(ACRES) = 34.2 PEAK FLOW RATE(CFS) = 90.71

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END OF SUBAREA "V" GUTTER HYDRAULICS:
DEPTH(FEET) = 0.60 FLOOD WIDTH(FEET) = 13.60
FLOW VELOCITY(FEET/SEC.) = 17.53 DEPTH*VELOCITY(FT*FT/SEC) = 10.48
LONGEST FLOWPATH FROM NODE 10.00 TO NODE 14.00 = 1942.00 FEET.

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FLOW PROCESS FROM NODE 14.00 TO NODE 14.00 IS CODE = 1
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>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
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TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 15.67
RAINFALL INTENSITY(INCH/HR) = 3.22
AREA-AVERAGED Fm(INCH/HR) = 0.27
AREA-AVERAGED Fp(INCH/HR) = 0.27
AREA-AVERAGED Ap = 1.00
EFFECTIVE STREAM AREA(ACRES) = 34.21
TOTAL STREAM AREA(ACRES) = 34.21
PEAK FLOW RATE(CFS) AT CONFLUENCE = 90.71

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FLOW PROCESS FROM NODE 31.00 TO NODE 32.00 IS CODE = 21
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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
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INITIAL SUBAREA FLOW-LENGTH(FEET) = 365.00
ELEVATION DATA: UPSTREAM(FEET) = 696.80 DOWNSTREAM(FEET) = 623.00

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Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 10.294
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.091

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SUBAREA Tc AND LOSS RATE DATA(AMC III):

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DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
NATURAL FAIR COVER						
"CHAPARRAL,NARROWLEAF"	B	0.48	0.30	1.000	89	10.29
NATURAL FAIR COVER						
"CHAPARRAL,NARROWLEAF"	C	1.87	0.25	1.000	95	10.29
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.26						
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000						
SUBAREA RUNOFF(CFS) = 8.10						
TOTAL AREA(ACRES) = 2.35 PEAK FLOW RATE(CFS) = 8.10						

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FLOW PROCESS FROM NODE 32.00 TO NODE 33.00 IS CODE = 31
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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

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>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

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ELEVATION DATA: UPSTREAM(FEET) = 618.00 DOWNSTREAM(FEET) = 601.00
FLOW LENGTH(FEET) = 116.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 7.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.02
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 8.10
PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 10.41
LONGEST FLOWPATH FROM NODE 31.00 TO NODE 33.00 = 481.00 FEET.

FLOW PROCESS FROM NODE 33.00 TO NODE 14.00 IS CODE = 91

>>>>COMPUTE "V" GUTTER FLOW TRAVEL TIME THRU SUBAREA<<<<<

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UPSTREAM NODE ELEVATION(FEET) = 601.00
DOWNSTREAM NODE ELEVATION(FEET) = 596.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 76.00
"V" GUTTER WIDTH(FEET) = 5.00 GUTTER HIKE(FEET) = 0.050
PAVEMENT LIP(FEET) = 0.010 MANNING'S N = .0500
PAVEMENT CROSSFALL(DECIMAL NOTATION) = 0.12500
MAXIMUM DEPTH(FEET) = 3.00
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.981
SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL FAIR COVER					
"CHAPARRAL,NARROWLEAF"	B	0.01	0.30	1.000	89

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 8.12
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.26
AVERAGE FLOW DEPTH(FEET) = 0.37 FLOOD WIDTH(FEET) = 9.95
"V" GUTTER FLOW TRAVEL TIME(MIN.) = 0.39 Tc(MIN.) = 10.80
SUBAREA AREA(ACRES) = 0.01 SUBAREA RUNOFF(CFS) = 0.03
EFFECTIVE AREA(ACRES) = 2.36 AREA-AVERAGED Fm(INCH/HR) = 0.26
AREA-AVERAGED Fp(INCH/HR) = 0.26 AREA-AVERAGED Ap = 1.00
TOTAL AREA(ACRES) = 2.4 PEAK FLOW RATE(CFS) = 8.10
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

END OF SUBAREA "V" GUTTER HYDRAULICS:
DEPTH(FEET) = 0.37 FLOOD WIDTH(FEET) = 9.95
FLOW VELOCITY(FEET/SEC.) = 3.26 DEPTH*VELOCITY(FT*FT/SEC) = 1.20
LONGEST FLOWPATH FROM NODE 31.00 TO NODE 14.00 = 557.00 FEET.

FLOW PROCESS FROM NODE 14.00 TO NODE 14.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 10.80
RAINFALL INTENSITY(INCH/HR) = 3.98
AREA-AVERAGED Fm(INCH/HR) = 0.26
AREA-AVERAGED Fp(INCH/HR) = 0.26
AREA-AVERAGED Ap = 1.00
EFFECTIVE STREAM AREA(ACRES) = 2.36
TOTAL STREAM AREA(ACRES) = 2.36
PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.10

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	90.71	15.67	3.216	0.27 (0.27)	1.00	34.2	10.00
2	8.10	10.80	3.981	0.26 (0.26)	1.00	2.4	31.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	86.84	10.80	3.981	0.27 (0.27)	1.00	25.9	31.00
2	97.15	15.67	3.216	0.27 (0.27)	1.00	36.6	10.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 97.15 Tc(MIN.) = 15.67
EFFECTIVE AREA(ACRES) = 36.57 AREA-AVERAGED Fm(INCH/HR) = 0.27
AREA-AVERAGED Fp(INCH/HR) = 0.27 AREA-AVERAGED Ap = 1.00
TOTAL AREA(ACRES) = 36.6
LONGEST FLOWPATH FROM NODE 10.00 TO NODE 14.00 = 1942.00 FEET.

FLOW PROCESS FROM NODE 14.00 TO NODE 15.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 596.00 DOWNSTREAM(FEET) = 590.00
FLOW LENGTH(FEET) = 82.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 30.0 INCH PIPE IS 23.3 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 23.71
ESTIMATED PIPE DIAMETER(INCH) = 30.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 97.15
PIPE TRAVEL TIME(MIN.) = 0.06 Tc(MIN.) = 15.72
LONGEST FLOWPATH FROM NODE 10.00 TO NODE 15.00 = 2024.00 FEET.

FLOW PROCESS FROM NODE 15.00 TO NODE 16.00 IS CODE = 91

>>>>COMPUTE "V" GUTTER FLOW TRAVEL TIME THRU SUBAREA<<<<<

=====

UPSTREAM NODE ELEVATION(FEET) = 590.00
DOWNSTREAM NODE ELEVATION(FEET) = 578.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 29.00
"V" GUTTER WIDTH(FEET) = 5.00 GUTTER HIKE(FEET) = 0.050
PAVEMENT LIP(FEET) = 0.010 MANNING'S N = .0500
PAVEMENT CROSSFALL(DECIMAL NOTATION) = 0.00200
MAXIMUM DEPTH(FEET) = 3.00
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.196
SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL GOOD COVER					
"WOODLAND"	B	0.01	0.30	1.000	75

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 97.16
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.33
AVERAGE FLOW DEPTH(FEET) = 0.27 FLOOD WIDTH(FEET) = 211.00
"V" GUTTER FLOW TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 15.84
SUBAREA AREA(ACRES) = 0.01 SUBAREA RUNOFF(CFS) = 0.03
EFFECTIVE AREA(ACRES) = 36.58 AREA-AVERAGED Fm(INCH/HR) = 0.27

AREA-AVERAGED Fp (INCH/HR) = 0.27 AREA-AVERAGED Ap = 1.00
 TOTAL AREA (ACRES) = 36.6 PEAK FLOW RATE (CFS) = 97.15
 NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

END OF SUBAREA "V" GUTTER HYDRAULICS:
 DEPTH (FEET) = 0.26 FLOOD WIDTH (FEET) = 209.57
 FLOW VELOCITY (FEET/SEC.) = 4.39 DEPTH*VELOCITY (FT*FT/SEC) = 1.16
 LONGEST FLOWPATH FROM NODE 10.00 TO NODE 16.00 = 2053.00 FEET.

 FLOW PROCESS FROM NODE 16.00 TO NODE 16.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

 FLOW PROCESS FROM NODE 50.00 TO NODE 51.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 297.00
 ELEVATION DATA: UPSTREAM (FEET) = 698.30 DOWNSTREAM (FEET) = 693.50

Tc = K * [(LENGTH** 3.00) / (ELEVATION CHANGE)]**0.20
 SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 11.683
 * 100 YEAR RAINFALL INTENSITY (INCH/HR) = 3.804
 SUBAREA Tc AND LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
NATURAL POOR COVER						
"GRASS"	C	0.30	0.25	1.000	97	11.68

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.25
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
 SUBAREA RUNOFF (CFS) = 0.96
 TOTAL AREA (ACRES) = 0.30 PEAK FLOW RATE (CFS) = 0.96

 FLOW PROCESS FROM NODE 51.00 TO NODE 52.00 IS CODE = 91

>>>>COMPUTE "V" GUTTER FLOW TRAVEL TIME THRU SUBAREA<<<<<

=====

UPSTREAM NODE ELEVATION (FEET) = 693.50
 DOWNSTREAM NODE ELEVATION (FEET) = 666.50
 CHANNEL LENGTH THRU SUBAREA (FEET) = 1046.00
 "V" GUTTER WIDTH (FEET) = 5.00 GUTTER HIKE (FEET) = 0.050
 PAVEMENT LIP (FEET) = 0.010 MANNING'S N = .0150
 PAVEMENT CROSSFALL (DECIMAL NOTATION) = 0.20000
 MAXIMUM DEPTH (FEET) = 3.00
 * 100 YEAR RAINFALL INTENSITY (INCH/HR) = 3.235
 SUBAREA LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL POOR COVER					
"GRASS"	C	2.50	0.25	1.000	97

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.25
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 4.10
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 4.56
 AVERAGE FLOW DEPTH (FEET) = 0.19 FLOOD WIDTH (FEET) = 6.28
 "V" GUTTER FLOW TRAVEL TIME (MIN.) = 3.82 Tc (MIN.) = 15.51
 SUBAREA AREA (ACRES) = 2.50 SUBAREA RUNOFF (CFS) = 6.72
 EFFECTIVE AREA (ACRES) = 2.80 AREA-AVERAGED Fm (INCH/HR) = 0.25

AREA-AVERAGED Fp (INCH/HR) = 0.25 AREA-AVERAGED Ap = 1.00
 TOTAL AREA (ACRES) = 2.8 PEAK FLOW RATE (CFS) = 7.52

END OF SUBAREA "V" GUTTER HYDRAULICS:

DEPTH (FEET) = 0.26 FLOOD WIDTH (FEET) = 6.96
 FLOW VELOCITY (FEET/SEC.) = 5.59 DEPTH*VELOCITY (FT*FT/SEC) = 1.43
 LONGEST FLOWPATH FROM NODE 50.00 TO NODE 52.00 = 1343.00 FEET.

 FLOW PROCESS FROM NODE 52.00 TO NODE 53.00 IS CODE = 91

 >>>>COMPUTE "V" GUTTER FLOW TRAVEL TIME THRU SUBAREA<<<<
 =====

UPSTREAM NODE ELEVATION (FEET) = 666.50
 DOWNSTREAM NODE ELEVATION (FEET) = 606.00
 CHANNEL LENGTH THRU SUBAREA (FEET) = 397.00
 "V" GUTTER WIDTH (FEET) = 5.00 GUTTER HIKE (FEET) = 0.050
 PAVEMENT LIP (FEET) = 0.010 MANNING'S N = .0150
 PAVEMENT CROSSFALL (DECIMAL NOTATION) = 0.20000
 MAXIMUM DEPTH (FEET) = 3.00
 * 100 YEAR RAINFALL INTENSITY (INCH/HR) = 3.168
 SUBAREA LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL POOR COVER "GRASS"	A	0.03	0.40	1.000	85
NATURAL POOR COVER "GRASS"	B	1.53	0.30	1.000	93
NATURAL POOR COVER "GRASS"	C	1.16	0.25	1.000	97
NATURAL POOR COVER "GRASS"	D	0.08	0.20	1.000	98

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.28
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 11.16
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 11.48
 AVERAGE FLOW DEPTH (FEET) = 0.20 FLOOD WIDTH (FEET) = 6.40
 "V" GUTTER FLOW TRAVEL TIME (MIN.) = 0.58 Tc (MIN.) = 16.08
 SUBAREA AREA (ACRES) = 2.80 SUBAREA RUNOFF (CFS) = 7.28
 EFFECTIVE AREA (ACRES) = 5.60 AREA-AVERAGED Fm (INCH/HR) = 0.26
 AREA-AVERAGED Fp (INCH/HR) = 0.26 AREA-AVERAGED Ap = 1.00
 TOTAL AREA (ACRES) = 5.6 PEAK FLOW RATE (CFS) = 14.64

END OF SUBAREA "V" GUTTER HYDRAULICS:

DEPTH (FEET) = 0.23 FLOOD WIDTH (FEET) = 6.69
 FLOW VELOCITY (FEET/SEC.) = 12.61 DEPTH*VELOCITY (FT*FT/SEC) = 2.88
 LONGEST FLOWPATH FROM NODE 50.00 TO NODE 53.00 = 1740.00 FEET.

 FLOW PROCESS FROM NODE 53.00 TO NODE 16.00 IS CODE = 91

 >>>>COMPUTE "V" GUTTER FLOW TRAVEL TIME THRU SUBAREA<<<<
 =====

UPSTREAM NODE ELEVATION (FEET) = 606.00
 DOWNSTREAM NODE ELEVATION (FEET) = 578.00
 CHANNEL LENGTH THRU SUBAREA (FEET) = 398.00
 "V" GUTTER WIDTH (FEET) = 5.00 GUTTER HIKE (FEET) = 0.050
 PAVEMENT LIP (FEET) = 0.010 MANNING'S N = .0500
 PAVEMENT CROSSFALL (DECIMAL NOTATION) = 0.20000
 MAXIMUM DEPTH (FEET) = 3.00
 * 100 YEAR RAINFALL INTENSITY (INCH/HR) = 3.016
 SUBAREA LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL POOR COVER "GRASS"	A	0.03	0.40	1.000	85
NATURAL POOR COVER "GRASS"	B	1.53	0.30	1.000	93
NATURAL POOR COVER "GRASS"	C	1.16	0.25	1.000	97
NATURAL POOR COVER "GRASS"	D	0.08	0.20	1.000	98

LAND USE	GROUP	(ACRES)	(INCH/HR)	(DECIMAL)	CN
NATURAL GOOD COVER "WOODLAND"	A	0.65	0.40	1.000	45
NATURAL GOOD COVER "WOODLAND"	B	2.13	0.30	1.000	75
NATURAL GOOD COVER "WOODLAND"	C	1.04	0.25	1.000	87

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 1.000
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 19.30
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 4.62
 AVERAGE FLOW DEPTH (FEET) = 0.58 FLOOD WIDTH (FEET) = 10.25
 "V" GUTTER FLOW TRAVEL TIME (MIN.) = 1.44 T_c (MIN.) = 17.52
 SUBAREA AREA (ACRES) = 3.82 SUBAREA RUNOFF (CFS) = 9.33
 EFFECTIVE AREA (ACRES) = 9.42 AREA-AVERAGED F_m (INCH/HR) = 0.28
 AREA-AVERAGED F_p (INCH/HR) = 0.28 AREA-AVERAGED A_p = 1.00
 TOTAL AREA (ACRES) = 9.4 PEAK FLOW RATE (CFS) = 23.20

END OF SUBAREA "V" GUTTER HYDRAULICS:
 DEPTH (FEET) = 0.64 FLOOD WIDTH (FEET) = 10.79
 FLOW VELOCITY (FEET/SEC.) = 4.89 DEPTH*VELOCITY (FT*FT/SEC) = 3.12
 LONGEST FLOWPATH FROM NODE 50.00 TO NODE 16.00 = 2138.00 FEET.

 FLOW PROCESS FROM NODE 16.00 TO NODE 16.00 IS CODE = 11

 >>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<
 =====

** MAIN STREAM CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	T_c (MIN.)	Intensity (INCH/HR)	F_p (F_m) (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	23.20	17.52	3.016	0.28 (0.28)	1.00	9.4	50.00

 LONGEST FLOWPATH FROM NODE 50.00 TO NODE 16.00 = 2138.00 FEET.

** MEMORY BANK # 1 CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	T_c (MIN.)	Intensity (INCH/HR)	F_p (F_m) (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	86.84	10.97	3.945	0.27 (0.27)	1.00	25.9	31.00
2	97.15	15.84	3.196	0.27 (0.27)	1.00	36.6	10.00

 LONGEST FLOWPATH FROM NODE 10.00 TO NODE 16.00 = 2053.00 FEET.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	T_c (MIN.)	Intensity (INCH/HR)	F_p (F_m) (INCH/HR)	A_p	A_e (ACRES)	HEADWATER NODE
1	106.29	10.97	3.945	0.27 (0.27)	1.00	31.8	31.00
2	119.50	15.84	3.196	0.27 (0.27)	1.00	45.1	10.00
3	114.39	17.52	3.016	0.27 (0.27)	1.00	46.0	50.00

 TOTAL AREA (ACRES) = 46.0

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:
 PEAK FLOW RATE (CFS) = 119.50 T_c (MIN.) = 15.835
 EFFECTIVE AREA (ACRES) = 45.10 AREA-AVERAGED F_m (INCH/HR) = 0.27
 AREA-AVERAGED F_p (INCH/HR) = 0.27 AREA-AVERAGED A_p = 1.00
 TOTAL AREA (ACRES) = 46.0
 LONGEST FLOWPATH FROM NODE 50.00 TO NODE 16.00 = 2138.00 FEET.

 FLOW PROCESS FROM NODE 16.00 TO NODE 16.00 IS CODE = 12

 >>>>CLEAR MEMORY BANK # 1 <<<<<
 =====

 FLOW PROCESS FROM NODE 16.00 TO NODE 17.00 IS CODE = 91

>>>>COMPUTE "V" GUTTER FLOW TRAVEL TIME THRU SUBAREA<<<<<

=====

UPSTREAM NODE ELEVATION(FEET) = 578.00
 DOWNSTREAM NODE ELEVATION(FEET) = 558.83
 CHANNEL LENGTH THRU SUBAREA(FEET) = 466.00
 "V" GUTTER WIDTH(FEET) = 5.00 GUTTER HIKE(FEET) = 0.050
 PAVEMENT LIP(FEET) = 0.010 MANNING'S N = .0500
 PAVEMENT CROSSFALL(DECIMAL NOTATION) = 0.20000
 MAXIMUM DEPTH(FEET) = 6.00
 * 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.060
 SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL GOOD COVER "WOODLAND"	A	1.58	0.40	1.000	45
NATURAL GOOD COVER "WOODLAND"	B	0.24	0.30	1.000	75
NATURAL GOOD COVER "WOODLAND"	C	0.63	0.25	1.000	87

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.35
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 122.49
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 6.24
 AVERAGE FLOW DEPTH(FEET) = 1.60 FLOOD WIDTH(FEET) = 20.35
 "V" GUTTER FLOW TRAVEL TIME(MIN.) = 1.24 Tc(MIN.) = 17.08
 SUBAREA AREA(ACRES) = 2.45 SUBAREA RUNOFF(CFS) = 5.97
 EFFECTIVE AREA(ACRES) = 47.55 AREA-AVERAGED Fm(INCH/HR) = 0.28
 AREA-AVERAGED Fp(INCH/HR) = 0.28 AREA-AVERAGED Ap = 1.00
 TOTAL AREA(ACRES) = 48.5 PEAK FLOW RATE(CFS) = 119.50
 NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

END OF SUBAREA "V" GUTTER HYDRAULICS:
 DEPTH(FEET) = 1.58 FLOOD WIDTH(FEET) = 20.18
 FLOW VELOCITY(FEET/SEC.) = 6.20 DEPTH*VELOCITY(FT*FT/SEC) = 9.78
 LONGEST FLOWPATH FROM NODE 50.00 TO NODE 17.00 = 2604.00 FEET.

 FLOW PROCESS FROM NODE 17.00 TO NODE 17.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

 FLOW PROCESS FROM NODE 40.00 TO NODE 41.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 614.00
 ELEVATION DATA: UPSTREAM(FEET) = 681.80 DOWNSTREAM(FEET) = 594.50

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 13.599
 * 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.487
 SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
NATURAL FAIR COVER "CHAPARRAL,NARROWLEAF"	A	0.33	0.40	1.000	75	13.60
NATURAL FAIR COVER						

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"CHAPARRAL,NARROWLEAF"   B      0.93    0.30    1.000    89    13.60
NATURAL FAIR COVER
"CHAPARRAL,NARROWLEAF"   C      1.30    0.25    1.000    95    13.60
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.29
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
SUBAREA RUNOFF(CFS) =      7.37
TOTAL AREA(ACRES) =      2.56    PEAK FLOW RATE(CFS) =      7.37

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*****
FLOW PROCESS FROM NODE      41.00 TO NODE      42.00 IS CODE = 31
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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
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ELEVATION DATA: UPSTREAM(FEET) = 594.50 DOWNSTREAM(FEET) = 567.10
FLOW LENGTH(FEET) = 131.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 5.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 19.03
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 7.37
PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 13.71
LONGEST FLOWPATH FROM NODE 40.00 TO NODE 42.00 = 745.00 FEET.

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*****
FLOW PROCESS FROM NODE      42.00 TO NODE      42.00 IS CODE = 10
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>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<
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*****
FLOW PROCESS FROM NODE      40.00 TO NODE      45.00 IS CODE = 21
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>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
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INITIAL SUBAREA FLOW-LENGTH(FEET) = 322.00
ELEVATION DATA: UPSTREAM(FEET) = 681.80 DOWNSTREAM(FEET) = 618.00

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$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 9.830

* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.200

SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
NATURAL FAIR COVER						
"CHAPARRAL,NARROWLEAF"	B	0.20	0.30	1.000	89	9.83
NATURAL FAIR COVER						
"CHAPARRAL,NARROWLEAF"	C	2.51	0.25	1.000	95	9.83
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.25						
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000						
SUBAREA RUNOFF(CFS) = 9.63						
TOTAL AREA(ACRES) = 2.71 PEAK FLOW RATE(CFS) = 9.63						

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*****
FLOW PROCESS FROM NODE      45.00 TO NODE      46.00 IS CODE = 31
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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
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ELEVATION DATA: UPSTREAM(FEET) = 615.00 DOWNSTREAM(FEET) = 609.29
FLOW LENGTH(FEET) = 306.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 11.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 8.16

```

ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 9.63
 PIPE TRAVEL TIME(MIN.) = 0.62 Tc(MIN.) = 10.45
 LONGEST FLOWPATH FROM NODE 40.00 TO NODE 46.00 = 628.00 FEET.

 FLOW PROCESS FROM NODE 46.00 TO NODE 46.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 10.45
 * 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.055
 SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	A	0.20	0.40	0.100	52
COMMERCIAL	B	0.58	0.30	0.100	76

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.33
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA AREA(ACRES) = 0.78 SUBAREA RUNOFF(CFS) = 2.82
 EFFECTIVE AREA(ACRES) = 3.49 AREA-AVERAGED Fm(INCH/HR) = 0.20
 AREA-AVERAGED Fp(INCH/HR) = 0.26 AREA-AVERAGED Ap = 0.80
 TOTAL AREA(ACRES) = 3.5 PEAK FLOW RATE(CFS) = 12.09

 FLOW PROCESS FROM NODE 46.00 TO NODE 47.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 609.29 DOWNSTREAM(FEET) = 571.50
 FLOW LENGTH(FEET) = 168.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 12.0 INCH PIPE IS 7.9 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 21.92
 ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 12.09
 PIPE TRAVEL TIME(MIN.) = 0.13 Tc(MIN.) = 10.58
 LONGEST FLOWPATH FROM NODE 40.00 TO NODE 47.00 = 796.00 FEET.

 FLOW PROCESS FROM NODE 47.00 TO NODE 47.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
 TIME OF CONCENTRATION(MIN.) = 10.58
 RAINFALL INTENSITY(INCH/HR) = 4.03
 AREA-AVERAGED Fm(INCH/HR) = 0.20
 AREA-AVERAGED Fp(INCH/HR) = 0.26
 AREA-AVERAGED Ap = 0.80
 EFFECTIVE STREAM AREA(ACRES) = 3.49
 TOTAL STREAM AREA(ACRES) = 3.49
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.09

 FLOW PROCESS FROM NODE 48.00 TO NODE 48.50 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 529.00
 ELEVATION DATA: UPSTREAM(FEET) = 628.80 DOWNSTREAM(FEET) = 582.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 10.476

* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.050

SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
NATURAL POOR COVER "CHAPARRAL,NARROWLEAF"	A	1.10	0.40	1.000	88	10.48
NATURAL POOR COVER "GRASS"	B	0.49	0.30	1.000	93	10.48

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.37
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
SUBAREA RUNOFF(CFS) = 5.27
TOTAL AREA(ACRES) = 1.59 PEAK FLOW RATE(CFS) = 5.27

FLOW PROCESS FROM NODE 48.50 TO NODE 47.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 577.00 DOWNSTREAM(FEET) = 571.50
FLOW LENGTH(FEET) = 132.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 12.0 INCH PIPE IS 8.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.45
ESTIMATED PIPE DIAMETER(INCH) = 12.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 5.27
PIPE TRAVEL TIME(MIN.) = 0.23 Tc(MIN.) = 10.71
LONGEST FLOWPATH FROM NODE 48.00 TO NODE 47.00 = 661.00 FEET.

FLOW PROCESS FROM NODE 47.00 TO NODE 47.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 10.71
RAINFALL INTENSITY(INCH/HR) = 4.00
AREA-AVERAGED Fm(INCH/HR) = 0.37
AREA-AVERAGED Fp(INCH/HR) = 0.37
AREA-AVERAGED Ap = 1.00
EFFECTIVE STREAM AREA(ACRES) = 1.59
TOTAL STREAM AREA(ACRES) = 1.59
PEAK FLOW RATE(CFS) AT CONFLUENCE = 5.27

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	12.09	10.58	4.026	0.26(0.20)	0.80	3.5	40.00
2	5.27	10.71	3.999	0.37(0.37)	1.00	1.6	48.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	17.34	10.58	4.026	0.30(0.26)	0.86	5.1	40.00
2	17.27	10.71	3.999	0.30(0.26)	0.86	5.1	48.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 17.34 Tc (MIN.) = 10.58
 EFFECTIVE AREA (ACRES) = 5.06 AREA-AVERAGED Fm (INCH/HR) = 0.26
 AREA-AVERAGED Fp (INCH/HR) = 0.30 AREA-AVERAGED Ap = 0.86
 TOTAL AREA (ACRES) = 5.1
 LONGEST FLOWPATH FROM NODE 40.00 TO NODE 47.00 = 796.00 FEET.

 FLOW PROCESS FROM NODE 47.00 TO NODE 49.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 571.50 DOWNSTREAM (FEET) = 568.38
 FLOW LENGTH (FEET) = 162.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.9 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 9.47
 ESTIMATED PIPE DIAMETER (INCH) = 21.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 17.34
 PIPE TRAVEL TIME (MIN.) = 0.29 Tc (MIN.) = 10.87
 LONGEST FLOWPATH FROM NODE 40.00 TO NODE 49.00 = 958.00 FEET.

 FLOW PROCESS FROM NODE 49.00 TO NODE 49.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc (MIN.) = 10.87
 * 100 YEAR RAINFALL INTENSITY (INCH/HR) = 3.966
 SUBAREA LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL FAIR COVER					
"CHAPARRAL, NARROWLEAF"	A	1.50	0.40	1.000	75
NATURAL FAIR COVER					
"CHAPARRAL, NARROWLEAF"	B	0.28	0.30	1.000	89
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.38					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000					
SUBAREA AREA (ACRES) = 1.78 SUBAREA RUNOFF (CFS) = 5.74					
EFFECTIVE AREA (ACRES) = 6.84 AREA-AVERAGED Fm (INCH/HR) = 0.29					
AREA-AVERAGED Fp (INCH/HR) = 0.32 AREA-AVERAGED Ap = 0.90					
TOTAL AREA (ACRES) = 6.9 PEAK FLOW RATE (CFS) = 22.64					

 FLOW PROCESS FROM NODE 49.00 TO NODE 42.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 568.38 DOWNSTREAM (FEET) = 567.10
 FLOW LENGTH (FEET) = 58.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 15.2 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 10.77
 ESTIMATED PIPE DIAMETER (INCH) = 24.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 22.64
 PIPE TRAVEL TIME (MIN.) = 0.09 Tc (MIN.) = 10.96
 LONGEST FLOWPATH FROM NODE 40.00 TO NODE 42.00 = 1016.00 FEET.

 FLOW PROCESS FROM NODE 42.00 TO NODE 42.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<

** MAIN STREAM CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	22.64	10.96	3.947	0.32(0.29)	0.90	6.8	40.00
2	22.54	11.08	3.921	0.32(0.29)	0.90	6.9	48.00

LONGEST FLOWPATH FROM NODE 40.00 TO NODE 42.00 = 1016.00 FEET.

** MEMORY BANK # 2 CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	7.37	13.71	3.471	0.29(0.29)	1.00	2.6	40.00

LONGEST FLOWPATH FROM NODE 40.00 TO NODE 42.00 = 745.00 FEET.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	29.41	10.96	3.947	0.31(0.29)	0.92	8.9	40.00
2	29.34	11.08	3.921	0.31(0.29)	0.92	8.9	48.00
3	27.11	13.71	3.471	0.31(0.29)	0.93	9.4	40.00

TOTAL AREA (ACRES) = 9.4

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 29.41 Tc (MIN.) = 10.957
 EFFECTIVE AREA (ACRES) = 8.89 AREA-AVERAGED Fm (INCH/HR) = 0.29
 AREA-AVERAGED Fp (INCH/HR) = 0.31 AREA-AVERAGED Ap = 0.92
 TOTAL AREA (ACRES) = 9.4
 LONGEST FLOWPATH FROM NODE 40.00 TO NODE 42.00 = 1016.00 FEET.

 FLOW PROCESS FROM NODE 42.00 TO NODE 42.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 2 <<<<<

 FLOW PROCESS FROM NODE 42.00 TO NODE 17.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM (FEET) = 567.10 DOWNSTREAM (FEET) = 558.83
 FLOW LENGTH (FEET) = 74.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 13.5 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 20.76
 ESTIMATED PIPE DIAMETER (INCH) = 18.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 29.41
 PIPE TRAVEL TIME (MIN.) = 0.06 Tc (MIN.) = 11.02
 LONGEST FLOWPATH FROM NODE 40.00 TO NODE 17.00 = 1090.00 FEET.

 FLOW PROCESS FROM NODE 17.00 TO NODE 17.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

** MAIN STREAM CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	29.41	11.02	3.935	0.31(0.29)	0.92	8.9	40.00
2	29.34	11.14	3.909	0.31(0.29)	0.92	8.9	48.00
3	27.11	13.77	3.462	0.31(0.29)	0.93	9.4	40.00

LONGEST FLOWPATH FROM NODE 40.00 TO NODE 17.00 = 1090.00 FEET.

** MEMORY BANK # 1 CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	106.29	12.25	3.703	0.28 (0.28)	1.00	34.3	31.00
2	119.50	17.08	3.060	0.28 (0.28)	1.00	47.5	10.00
3	114.40	18.78	2.899	0.28 (0.28)	1.00	48.5	50.00

LONGEST FLOWPATH FROM NODE 50.00 TO NODE 17.00 = 2604.00 FEET.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	131.49	11.02	3.935	0.28 (0.28)	0.98	39.7	40.00
2	131.86	11.14	3.909	0.28 (0.28)	0.98	40.1	48.00
3	134.70	12.25	3.703	0.28 (0.28)	0.98	43.4	31.00
4	137.58	13.77	3.462	0.28 (0.28)	0.99	47.9	40.00
5	143.18	17.08	3.060	0.28 (0.28)	0.99	57.0	10.00
6	136.70	18.78	2.899	0.28 (0.28)	0.99	57.9	50.00

TOTAL AREA(ACRES) = 57.9

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 143.18 Tc(MIN.) = 17.080
 EFFECTIVE AREA(ACRES) = 56.97 AREA-AVERAGED Fm(INCH/HR) = 0.28
 AREA-AVERAGED Fp(INCH/HR) = 0.28 AREA-AVERAGED Ap = 0.99
 TOTAL AREA(ACRES) = 57.9
 LONGEST FLOWPATH FROM NODE 50.00 TO NODE 17.00 = 2604.00 FEET.

 FLOW PROCESS FROM NODE 17.00 TO NODE 17.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

 FLOW PROCESS FROM NODE 17.00 TO NODE 18.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 558.83 DOWNSTREAM(FEET) = 557.94
 FLOW LENGTH(FEET) = 160.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 57.0 INCH PIPE IS 42.9 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 10.00
 ESTIMATED PIPE DIAMETER(INCH) = 57.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 143.18
 PIPE TRAVEL TIME(MIN.) = 0.27 Tc(MIN.) = 17.35
 LONGEST FLOWPATH FROM NODE 50.00 TO NODE 18.00 = 2764.00 FEET.

 FLOW PROCESS FROM NODE 18.00 TO NODE 18.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 17.35
 * 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.033
 SUBAREA LOSS RATE DATA(AMC III):
 DEVELOPMENT TYPE/ LAND USE SCS SOIL GROUP AREA (ACRES) Fp (INCH/HR) Ap (DECIMAL) SCS CN
 NATURAL GOOD COVER
 "CHAPARRAL, BROADLEAF" A 1.71 0.40 1.000 51
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.40
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
 SUBAREA AREA(ACRES) = 1.71 SUBAREA RUNOFF(CFS) = 4.05

EFFECTIVE AREA (ACRES) = 58.68 AREA-AVERAGED Fm (INCH/HR) = 0.28
 AREA-AVERAGED Fp (INCH/HR) = 0.28 AREA-AVERAGED Ap = 0.99
 TOTAL AREA (ACRES) = 59.6 PEAK FLOW RATE (CFS) = 145.35

=====
 END OF STUDY SUMMARY:

TOTAL AREA (ACRES) = 59.6 TC (MIN.) = 17.35
 EFFECTIVE AREA (ACRES) = 58.68 AREA-AVERAGED Fm (INCH/HR) = 0.28
 AREA-AVERAGED Fp (INCH/HR) = 0.28 AREA-AVERAGED Ap = 0.988
 PEAK FLOW RATE (CFS) = 145.35

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	134.10	11.29	3.879	0.29 (0.28)	0.98	41.4	40.00
2	134.45	11.42	3.855	0.29 (0.28)	0.98	41.8	48.00
3	137.00	12.52	3.656	0.29 (0.28)	0.98	45.1	31.00
4	140.25	14.04	3.424	0.29 (0.28)	0.99	49.6	40.00
5	145.35	17.35	3.033	0.28 (0.28)	0.99	58.7	10.00
6	139.12	19.05	2.875	0.28 (0.28)	0.99	59.6	50.00

=====
 END OF RATIONAL METHOD ANALYSIS

EXISTING AREA B

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
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Ver. 13.5 Release Date: 02/06/2007 License ID 1355

Analysis prepared by:

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***** DESCRIPTION OF STUDY *****
* IRWD SITE - AREA B *
* 100 YEAR EXISTING HYDROLOGY *
* 6/9/08 JEL *

FILE NAME: IRWD00B.DAT
TIME/DATE OF STUDY: 12:04 06/09/2008

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:
=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT (YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE (INCH) = 18.00
SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.95
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL IN- / OUT- / SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER WIDTH (FT)	GEOMETRIES LIP (FT)	MANNING HIKE (FT)	FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 60.00 TO NODE 61.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 240.00
ELEVATION DATA: UPSTREAM (FEET) = 679.70 DOWNSTREAM (FEET) = 673.60

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 5.675
* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 5.754
SUBAREA T_c AND LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
-------------------------------	-------------------	-----------------	--------------------	--------------------	-----------	-----------------

COMMERCIAL C 2.04 0.25 0.100 86 5.67
 SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.25
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 0.100
 SUBAREA RUNOFF(CFS) = 10.52
 TOTAL AREA(ACRES) = 2.04 PEAK FLOW RATE(CFS) = 10.52

 FLOW PROCESS FROM NODE 61.00 TO NODE 62.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 673.60 DOWNSTREAM(FEET) = 637.00
 FLOW LENGTH(FEET) = 540.00 MANNING'S N = 0.013
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 7.9 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 14.20
 ESTIMATED PIPE DIAMETER(INCH) = 18.000 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 10.52
 PIPE TRAVEL TIME(MIN.) = 0.63 T_c (MIN.) = 6.31
 LONGEST FLOWPATH FROM NODE 60.00 TO NODE 62.00 = 780.00 FEET.

 FLOW PROCESS FROM NODE 62.00 TO NODE 62.50 IS CODE = 91

>>>>COMPUTE "V" GUTTER FLOW TRAVEL TIME THRU SUBAREA<<<<<

=====

UPSTREAM NODE ELEVATION(FEET) = 637.00
 DOWNSTREAM NODE ELEVATION(FEET) = 624.00
 CHANNEL LENGTH THRU SUBAREA(FEET) = 62.00
 "V" GUTTER WIDTH(FEET) = 5.00 GUTTER HIKE(FEET) = 0.050
 PAVEMENT LIP(FEET) = 0.010 MANNING'S N = .0150
 PAVEMENT CROSSFALL(DECIMAL NOTATION) = 0.12500
 MAXIMUM DEPTH(FEET) = 3.00
 * 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.378
 SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN
NATURAL POOR COVER "GRASS"	B	0.11	0.30	1.000	93
NATURAL POOR COVER "GRASS"	C	1.36	0.25	1.000	97

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.25
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 1.000
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 13.91
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 13.22
 AVERAGE FLOW DEPTH(FEET) = 0.20 FLOOD WIDTH(FEET) = 7.29
 "V" GUTTER FLOW TRAVEL TIME(MIN.) = 0.08 T_c (MIN.) = 6.39
 SUBAREA AREA(ACRES) = 1.47 SUBAREA RUNOFF(CFS) = 6.78
 EFFECTIVE AREA(ACRES) = 3.51 AREA-AVERAGED F_m (INCH/HR) = 0.12
 AREA-AVERAGED F_p (INCH/HR) = 0.25 AREA-AVERAGED A_p = 0.48
 TOTAL AREA(ACRES) = 3.5 PEAK FLOW RATE(CFS) = 16.61

END OF SUBAREA "V" GUTTER HYDRAULICS:
 DEPTH(FEET) = 0.22 FLOOD WIDTH(FEET) = 7.56
 FLOW VELOCITY(FEET/SEC.) = 14.07 DEPTH*VELOCITY(FT*FT/SEC) = 3.10
 LONGEST FLOWPATH FROM NODE 60.00 TO NODE 62.50 = 842.00 FEET.

 FLOW PROCESS FROM NODE 62.50 TO NODE 63.00 IS CODE = 91

>>>>COMPUTE "V" GUTTER FLOW TRAVEL TIME THRU SUBAREA<<<<<

=====

UPSTREAM NODE ELEVATION(FEET) = 624.00
 DOWNSTREAM NODE ELEVATION(FEET) = 613.00
 CHANNEL LENGTH THRU SUBAREA(FEET) = 192.00
 "V" GUTTER WIDTH(FEET) = 5.00 GUTTER HIKE(FEET) = 0.050
 PAVEMENT LIP(FEET) = 0.010 MANNING'S N = .0500
 PAVEMENT CROSSFALL(DECIMAL NOTATION) = 0.12500
 MAXIMUM DEPTH(FEET) = 3.00
 * 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.052
 SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL POOR COVER "GRASS"	B	1.41	0.30	1.000	93
NATURAL POOR COVER "GRASS"	C	3.92	0.25	1.000	97

 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.26
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 28.03
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 4.35
 AVERAGE FLOW DEPTH(FEET) = 0.69 FLOOD WIDTH(FEET) = 15.03
 "V" GUTTER FLOW TRAVEL TIME(MIN.) = 0.74 Tc(MIN.) = 7.12
 SUBAREA AREA(ACRES) = 5.33 SUBAREA RUNOFF(CFS) = 22.97
 EFFECTIVE AREA(ACRES) = 8.84 AREA-AVERAGED Fm(INCH/HR) = 0.21
 AREA-AVERAGED Fp(INCH/HR) = 0.26 AREA-AVERAGED Ap = 0.79
 TOTAL AREA(ACRES) = 8.8 PEAK FLOW RATE(CFS) = 38.55

END OF SUBAREA "V" GUTTER HYDRAULICS:
 DEPTH(FEET) = 0.79 FLOOD WIDTH(FEET) = 16.75
 FLOW VELOCITY(FEET/SEC.) = 4.72 DEPTH*VELOCITY(FT*FT/SEC) = 3.75
 LONGEST FLOWPATH FROM NODE 60.00 TO NODE 63.00 = 1034.00 FEET.

 FLOW PROCESS FROM NODE 63.00 TO NODE 64.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
 =====
 ELEVATION DATA: UPSTREAM(FEET) = 613.00 DOWNSTREAM(FEET) = 607.80
 FLOW LENGTH(FEET) = 108.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 24.0 INCH PIPE IS 16.2 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 17.10
 ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 38.55
 PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 7.23
 LONGEST FLOWPATH FROM NODE 60.00 TO NODE 64.00 = 1142.00 FEET.

 FLOW PROCESS FROM NODE 64.00 TO NODE 64.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<
 =====
 MAINLINE Tc(MIN.) = 7.23
 * 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.009
 SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL POOR COVER "GRASS"	B	0.01	0.30	1.000	93
NATURAL POOR COVER "GRASS"	C	0.77	0.25	1.000	97

 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.25
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
 SUBAREA AREA(ACRES) = 0.78 SUBAREA RUNOFF(CFS) = 3.34

EFFECTIVE AREA (ACRES) = 9.62 AREA-AVERAGED Fm (INCH/HR) = 0.21
 AREA-AVERAGED Fp (INCH/HR) = 0.26 AREA-AVERAGED Ap = 0.81
 TOTAL AREA (ACRES) = 9.6 PEAK FLOW RATE (CFS) = 41.55

 FLOW PROCESS FROM NODE 64.00 TO NODE 65.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) =	607.80	DOWNSTREAM (FEET) =	582.15
FLOW LENGTH (FEET) =	416.00	MANNING'S N =	0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS	15.6	INCHES	
PIPE-FLOW VELOCITY (FEET/SEC.) =	19.17		
ESTIMATED PIPE DIAMETER (INCH) =	24.00	NUMBER OF PIPES =	1
PIPE-FLOW (CFS) =	41.55		
PIPE TRAVEL TIME (MIN.) =	0.36	Tc (MIN.) =	7.59
LONGEST FLOWPATH FROM NODE	60.00 TO NODE	65.00 =	1558.00 FEET.

 FLOW PROCESS FROM NODE 65.00 TO NODE 65.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc (MIN.) =	7.59				
* 100 YEAR RAINFALL INTENSITY (INCH/HR) =	4.871				
SUBAREA LOSS RATE DATA (AMC III):					
DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL POOR COVER "GRASS"	B	0.99	0.30	1.000	93
NATURAL POOR COVER "GRASS"	C	0.30	0.25	1.000	97
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.29					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000					
SUBAREA AREA (ACRES) =	1.29	SUBAREA RUNOFF (CFS) = 5.32			
EFFECTIVE AREA (ACRES) =	10.91	AREA-AVERAGED Fm (INCH/HR) = 0.22			
AREA-AVERAGED Fp (INCH/HR) =	0.26	AREA-AVERAGED Ap = 0.83			
TOTAL AREA (ACRES) =	10.9	PEAK FLOW RATE (CFS) = 45.67			

 FLOW PROCESS FROM NODE 65.00 TO NODE 65.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS =	2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:	
TIME OF CONCENTRATION (MIN.) =	7.59
RAINFALL INTENSITY (INCH/HR) =	4.87
AREA-AVERAGED Fm (INCH/HR) =	0.22
AREA-AVERAGED Fp (INCH/HR) =	0.26
AREA-AVERAGED Ap =	0.83
EFFECTIVE STREAM AREA (ACRES) =	10.91
TOTAL STREAM AREA (ACRES) =	10.91
PEAK FLOW RATE (CFS) AT CONFLUENCE =	45.67

 FLOW PROCESS FROM NODE 70.00 TO NODE 71.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) =	572.00
--------------------------------------	--------

ELEVATION DATA: UPSTREAM(FEET) = 644.70 DOWNSTREAM(FEET) = 593.80

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 14.518

* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.359

SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
NATURAL FAIR COVER "GRASS"	B	1.93	0.30	1.000	86	14.52
NATURAL FAIR COVER "GRASS"	C	0.97	0.25	1.000	93	14.52
NATURAL FAIR COVER "GRASS"	D	0.04	0.20	1.000	96	14.52

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.28

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000

SUBAREA RUNOFF(CFS) = 8.14

TOTAL AREA(ACRES) = 2.94 PEAK FLOW RATE(CFS) = 8.14

FLOW PROCESS FROM NODE 71.00 TO NODE 72.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====
ELEVATION DATA: UPSTREAM(FEET) = 589.80 DOWNSTREAM(FEET) = 583.00
FLOW LENGTH(FEET) = 266.00 MANNING'S N = 0.013
ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 9.25
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 8.14
PIPE TRAVEL TIME(MIN.) = 0.48 Tc(MIN.) = 15.00
LONGEST FLOWPATH FROM NODE 70.00 TO NODE 72.00 = 838.00 FEET.

FLOW PROCESS FROM NODE 72.00 TO NODE 72.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====
MAINLINE Tc(MIN.) = 15.00
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.297
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/
LAND USE SCS SOIL AREA Fp Ap SCS
GROUP (ACRES) (INCH/HR) (DECIMAL) CN
NATURAL GOOD COVER
"GRASS" A 0.10 0.40 1.000 58
NATURAL GOOD COVER
"GRASS" B 1.19 0.30 1.000 80
NATURAL GOOD COVER
"GRASS" C 0.26 0.25 1.000 90
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
SUBAREA AREA(ACRES) = 1.55 SUBAREA RUNOFF(CFS) = 4.18
EFFECTIVE AREA(ACRES) = 4.49 AREA-AVERAGED Fm(INCH/HR) = 0.29
AREA-AVERAGED Fp(INCH/HR) = 0.29 AREA-AVERAGED Ap = 1.00
TOTAL AREA(ACRES) = 4.5 PEAK FLOW RATE(CFS) = 12.16

FLOW PROCESS FROM NODE 72.00 TO NODE 65.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

```

=====
ELEVATION DATA: UPSTREAM(FEET) = 583.00 DOWNSTREAM(FEET) = 582.15
FLOW LENGTH(FEET) = 128.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 16.6 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 5.96
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 12.16
PIPE TRAVEL TIME(MIN.) = 0.36 Tc(MIN.) = 15.35
LONGEST FLOWPATH FROM NODE 70.00 TO NODE 65.00 = 966.00 FEET.

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*****
FLOW PROCESS FROM NODE 65.00 TO NODE 65.00 IS CODE = 1
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>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
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TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 15.35
RAINFALL INTENSITY(INCH/HR) = 3.25
AREA-AVERAGED Fm(INCH/HR) = 0.29
AREA-AVERAGED Fp(INCH/HR) = 0.29
AREA-AVERAGED Ap = 1.00
EFFECTIVE STREAM AREA(ACRES) = 4.49
TOTAL STREAM AREA(ACRES) = 4.49
PEAK FLOW RATE(CFS) AT CONFLUENCE = 12.16

```

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	45.67	7.59	4.871	0.26(0.22)	0.83	10.9	60.00
2	12.16	15.35	3.253	0.29(0.29)	1.00	4.5	70.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	54.97	7.59	4.871	0.27(0.23)	0.86	13.1	60.00
2	41.95	15.35	3.253	0.27(0.24)	0.88	15.4	70.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

```

PEAK FLOW RATE(CFS) = 54.97 Tc(MIN.) = 7.59
EFFECTIVE AREA(ACRES) = 13.13 AREA-AVERAGED Fm(INCH/HR) = 0.23
AREA-AVERAGED Fp(INCH/HR) = 0.27 AREA-AVERAGED Ap = 0.86
TOTAL AREA(ACRES) = 15.4
LONGEST FLOWPATH FROM NODE 60.00 TO NODE 65.00 = 1558.00 FEET.

```

```

*****
FLOW PROCESS FROM NODE 65.00 TO NODE 66.00 IS CODE = 31
-----

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>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
-----

```

```

ELEVATION DATA: UPSTREAM(FEET) = 582.15 DOWNSTREAM(FEET) = 563.50
FLOW LENGTH(FEET) = 278.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS 18.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 20.70
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 54.97
PIPE TRAVEL TIME(MIN.) = 0.22 Tc(MIN.) = 7.81
LONGEST FLOWPATH FROM NODE 60.00 TO NODE 66.00 = 1836.00 FEET.

```

FLOW PROCESS FROM NODE 66.00 TO NODE 67.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) =	563.50	DOWNSTREAM(FEET) =	562.00
FLOW LENGTH(FEET) =	185.00	MANNING'S N =	0.013
DEPTH OF FLOW IN	36.0 INCH PIPE IS	27.7 INCHES	
PIPE-FLOW VELOCITY(FEET/SEC.) =	9.41		
ESTIMATED PIPE DIAMETER(INCH) =	36.00	NUMBER OF PIPES =	1
PIPE-FLOW(CFS) =	54.97		
PIPE TRAVEL TIME(MIN.) =	0.33	Tc(MIN.) =	8.14
LONGEST FLOWPATH FROM NODE	60.00 TO NODE	67.00 =	2021.00 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) =	15.4	TC(MIN.) =	8.14
EFFECTIVE AREA(ACRES) =	13.13	AREA-AVERAGED Fm(INCH/HR) =	0.23
AREA-AVERAGED Fp(INCH/HR) =	0.27	AREA-AVERAGED Ap =	0.860
PEAK FLOW RATE(CFS) =	54.97		

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	54.97	8.14	4.679	0.27(0.23)	0.86	13.1	60.00
2	41.95	15.94	3.184	0.27(0.24)	0.88	15.4	70.00

END OF RATIONAL METHOD ANALYSIS

EXISTING OFFSITE 8

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
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Analysis prepared by:

Fusco Engineering, Inc
16795 Von Karman Suite 100, Irvine Ca 92606

***** DESCRIPTION OF STUDY *****
* IRWD SITE - AREA OFF-SITE 8 TO TRACT 15594 *
* 100 YEAR EXISTING HYDROLOGY *
* 6/9/08 JEL *

FILE NAME: IRW000S8.DAT
TIME/DATE OF STUDY: 15:47 06/09/2008

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 8.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.85
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT-/PARK- SIDE / SIDE/ WAY	CURB HEIGHT (FT)	GUTTER-GEOMETRIES: WIDTH LIP (FT) (FT)	MANNING HIKE FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00 0.0313	0.167 0.0150
2	14.0	9.0	0.020/0.020/0.050	0.33	2.00 0.0313	0.100 0.0140

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.33 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 90.00 TO NODE 91.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 332.00
ELEVATION DATA: UPSTREAM(FEET) = 693.40 DOWNSTREAM(FEET) = 625.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 13.076
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.567
SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/	SCS SOIL	AREA	Fp	Ap	SCS	Tc
-------------------	----------	------	----	----	-----	----

LAND USE	GROUP	(ACRES)	(INCH/HR)	(DECIMAL)	CN	(MIN.)
NATURAL GOOD COVER "OPEN BRUSH"	C	2.68	0.25	1.000	91	13.08
NATURAL GOOD COVER "OPEN BRUSH"	D	1.62	0.20	1.000	95	13.08
SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.23						
SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 1.000						
SUBAREA RUNOFF(CFS) = 12.91						
TOTAL AREA(ACRES) = 4.30 PEAK FLOW RATE(CFS) = 12.91						

=====

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 4.3 TC(MIN.) = 13.08
EFFECTIVE AREA(ACRES) = 4.30 AREA-AVERAGED F_m (INCH/HR) = 0.23
AREA-AVERAGED F_p (INCH/HR) = 0.23 AREA-AVERAGED A_p = 1.000
PEAK FLOW RATE(CFS) = 12.91

=====

=====

END OF RATIONAL METHOD ANALYSIS

EXISTING OFFSITE 9

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Analysis prepared by:

Fusco Engineering, Inc
16795 Von Karman Suite 100, Irvine Ca 92606

***** DESCRIPTION OF STUDY *****
* IRWD SITE - AREA OFF-SITE 9 TO OFF-SITE AREA *
* 100 YEAR EXISTING HYDROLOGY *
* 6/9/08 JEL *

FILE NAME: IRW000S9.DAT
TIME/DATE OF STUDY: 15:48 06/09/2008

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT (YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE (INCH) = 8.00
SPECIFIED PERCENT OF GRADIENTS (DECIMAL) TO USE FOR FRICTION SLOPE = 0.85
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF-WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT- / SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER WIDTH (FT)	GEOMETRIES: LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150
2	14.0	9.0	0.020/0.020/0.050	0.33	2.00	0.0313	0.100	0.0140

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.33 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)

SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.

*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 95.00 TO NODE 96.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 587.00
ELEVATION DATA: UPSTREAM (FEET) = 700.00 DOWNSTREAM (FEET) = 660.00

Tc = K * [(LENGTH** 3.00) / (ELEVATION CHANGE)] ** 0.20

SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 20.492

* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 2.757

SUBAREA Tc AND LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/	SCS SOIL	AREA	Fp	Ap	SCS	Tc
-------------------	----------	------	----	----	-----	----

LAND USE	GROUP	(ACRES)	(INCH/HR)	(DECIMAL)	CN	(MIN.)
NATURAL GOOD COVER						
"OPEN BRUSH"	C	2.02	0.25	1.000	91	20.49
NATURAL GOOD COVER						
"OPEN BRUSH"	D	0.08	0.20	1.000	95	20.49
SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.25						
SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 1.000						
SUBAREA RUNOFF(CFS) = 4.74						
TOTAL AREA(ACRES) = 2.10 PEAK FLOW RATE(CFS) = 4.74						

=====
 END OF STUDY SUMMARY:
 TOTAL AREA(ACRES) = 2.1 TC(MIN.) = 20.49
 EFFECTIVE AREA(ACRES) = 2.10 AREA-AVERAGED F_m (INCH/HR) = 0.25
 AREA-AVERAGED F_p (INCH/HR) = 0.25 AREA-AVERAGED A_p = 1.000
 PEAK FLOW RATE(CFS) = 4.74
 =====

=====
 END OF RATIONAL METHOD ANALYSIS

RATIONAL PROPOSED AREA A

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Analysis prepared by:

Fusco Engineering
16795 Von Karman Suite 100 Irvine Ca 92606

***** DESCRIPTION OF STUDY *****
* I.R.W.D. - LAKE FOREST SITE *
* PROPOSED 100 YEAR HYDROLOGY STUDY RESIDENTIAL AREA "A" *
* DEVELOPER: LEWIS OPERATING CORP *

FILE NAME: IRWD100.DAT
TIME/DATE OF STUDY: 10:46 07/14/2009

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.85
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF-WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT- / SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER WIDTH (FT)	LIP (FT)	HIKE (FT)	MANNING FACTOR (n)
1	18.0	13.0	0.020/0.020/0.020	0.50	1.50	0.0313	0.125	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 6.00 TO NODE 7.00 IS CODE = 21 ✓

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 295.00
ELEVATION DATA: UPSTREAM(FEET) = 692.10 DOWNSTREAM(FEET) = 689.30

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.998
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.727

SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL "11+ DWELLINGS/ACRE"	C	1.97	0.25	0.200	86	8.00

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.25
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA RUNOFF(CFS) = 8.29
TOTAL AREA(ACRES) = 1.97 PEAK FLOW RATE(CFS) = 8.29

FLOW PROCESS FROM NODE 7.00 TO NODE 8.00 IS CODE = 56 ✓

>>>>COMPUTE TRAPEZOIDAL CHANNEL FLOW<<<<<
>>>>TRAVELTIME THRU SUBAREA<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 689.30 DOWNSTREAM(FEET) = 683.80
CHANNEL LENGTH THRU SUBAREA(FEET) = 320.00 CHANNEL SLOPE = 0.0172
GIVEN CHANNEL BASE(FEET) = 120.00 CHANNEL FREEBOARD(FEET) = 0.1
"Z" FACTOR = 0.100 MANNING'S FACTOR = 0.030
*ESTIMATED CHANNEL HEIGHT(FEET) = 0.22
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.844
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"11+ DWELLINGS/ACRE" C 7.10 0.25 0.200 86
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.25
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 20.53
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 1.53
AVERAGE FLOW DEPTH(FEET) = 0.11 TRAVEL TIME(MIN.) = 3.48
Tc(MIN.) = 11.48
SUBAREA AREA(ACRES) = 7.10 SUBAREA RUNOFF(CFS) = 24.24
EFFECTIVE AREA(ACRES) = 9.07 AREA-AVERAGED Fm(INCH/HR) = 0.05
AREA-AVERAGED Fp(INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.20
TOTAL AREA(ACRES) = 9.1 PEAK FLOW RATE(CFS) = 30.97
GIVEN CHANNEL BASE(FEET) = 120.00 CHANNEL FREEBOARD(FEET) = 0.1
"Z" FACTOR = 0.100 MANNING'S FACTOR = 0.030
*ESTIMATED CHANNEL HEIGHT(FEET) = 0.24

END OF SUBAREA CHANNEL FLOW HYDRAULICS:
DEPTH(FEET) = 0.14 FLOW VELOCITY(FEET/SEC.) = 1.82
LONGEST FLOWPATH FROM NODE 6.00 TO NODE 8.00 = 615.00 FEET.

FLOW PROCESS FROM NODE 8.00 TO NODE 9.00 IS CODE = 31 ✓

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 676.70 DOWNSTREAM(FEET) = 654.30
FLOW LENGTH(FEET) = 510.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 24.0 INCH PIPE IS 14.9 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 15.09
ESTIMATED PIPE DIAMETER(INCH) = 24.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 30.97
PIPE TRAVEL TIME(MIN.) = 0.56 Tc(MIN.) = 12.04
LONGEST FLOWPATH FROM NODE 6.00 TO NODE 9.00 = 1125.00 FEET.

FLOW PROCESS FROM NODE 9.00 TO NODE 9.00 IS CODE = 1 ✓

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 12.04
RAINFALL INTENSITY(INCH/HR) = 3.74
AREA-AVERAGED Fm(INCH/HR) = 0.05
AREA-AVERAGED Fp(INCH/HR) = 0.25
AREA-AVERAGED Ap = 0.20
EFFECTIVE STREAM AREA(ACRES) = 9.07
TOTAL STREAM AREA(ACRES) = 9.07
PEAK FLOW RATE(CFS) AT CONFLUENCE = 30.97

```

*****
FLOW PROCESS FROM NODE      10.00 TO NODE      11.00 IS CODE = 21 ✓
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 186.00
ELEVATION DATA: UPSTREAM(FEET) = 691.00 DOWNSTREAM(FEET) = 689.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.487
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.330
SUBAREA Tc AND LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp      Ap      SCS  Tc
LAND USE              GROUP   (ACRES)  (INCH/HR) (DECIMAL) CN (MIN.)
RESIDENTIAL
"11+ DWELLINGS/ACRE"   C       0.75     0.25     0.200    86   6.49
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.25
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA RUNOFF(CFS) = 3.56
TOTAL AREA(ACRES) = 0.75 PEAK FLOW RATE(CFS) = 3.56

*****
FLOW PROCESS FROM NODE      11.00 TO NODE      12.00 IS CODE = 81 ✓
-----
>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<
=====
MAINLINE Tc(MIN.) = 6.49
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.330
SUBAREA LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/      SCS SOIL  AREA      Fp      Ap      SCS
LAND USE              GROUP   (ACRES)  (INCH/HR) (DECIMAL) CN
RESIDENTIAL
"11+ DWELLINGS/ACRE"   C       0.98     0.25     0.200    86
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.25
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA AREA(ACRES) = 0.98 SUBAREA RUNOFF(CFS) = 4.66
EFFECTIVE AREA(ACRES) = 1.73 AREA-AVERAGED Fm(INCH/HR) = 0.05
AREA-AVERAGED Fp(INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.20
TOTAL AREA(ACRES) = 1.7 PEAK FLOW RATE(CFS) = 8.22

*****
FLOW PROCESS FROM NODE      12.00 TO NODE      9.00 IS CODE = 31 ✓
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 654.70 DOWNSTREAM(FEET) = 654.30
FLOW LENGTH(FEET) = 80.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 14.2 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 4.77
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 8.22
PIPE TRAVEL TIME(MIN.) = 0.28 Tc(MIN.) = 6.77
LONGEST FLOWPATH FROM NODE 10.00 TO NODE 9.00 = 266.00 FEET.

*****
FLOW PROCESS FROM NODE      9.00 TO NODE      9.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 6.77
RAINFALL INTENSITY(INCH/HR) = 5.20
AREA-AVERAGED Fm(INCH/HR) = 0.05
AREA-AVERAGED Fp(INCH/HR) = 0.25
AREA-AVERAGED Ap = 0.20

```

EFFECTIVE STREAM AREA(ACRES) = 1.73
 TOTAL STREAM AREA(ACRES) = 1.73
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.22

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	30.97	12.04	3.740	0.25 (0.05)	0.20	9.1	6.00
2	8.22	6.77	5.202	0.25 (0.05)	0.20	1.7	10.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	32.53	6.77	5.202	0.25 (0.05)	0.20	6.8	10.00
2	36.85	12.04	3.740	0.25 (0.05)	0.20	10.8	6.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 36.85 Tc(MIN.) = 12.04
 EFFECTIVE AREA(ACRES) = 10.80 AREA-AVERAGED Fm(INCH/HR) = 0.05
 AREA-AVERAGED Fp(INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.20
 TOTAL AREA(ACRES) = 10.8
 LONGEST FLOWPATH FROM NODE 6.00 TO NODE 9.00 = 1125.00 FEET.

 FLOW PROCESS FROM NODE 9.00 TO NODE 13.00 IS CODE = 31 ✓

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW) <<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 654.30 DOWNSTREAM(FEET) = 652.00
 FLOW LENGTH(FEET) = 450.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 36.0 INCH PIPE IS 25.2 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 6.97
 ESTIMATED PIPE DIAMETER(INCH) = 36.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 36.85
 PIPE TRAVEL TIME(MIN.) = 1.08 Tc(MIN.) = 13.12
 LONGEST FLOWPATH FROM NODE 6.00 TO NODE 13.00 = 1575.00 FEET.

 FLOW PROCESS FROM NODE 13.00 TO NODE 13.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
 TIME OF CONCENTRATION(MIN.) = 13.12 ✓
 RAINFALL INTENSITY(INCH/HR) = 3.56
 AREA-AVERAGED Fm(INCH/HR) = 0.05
 AREA-AVERAGED Fp(INCH/HR) = 0.25
 AREA-AVERAGED Ap = 0.20
 EFFECTIVE STREAM AREA(ACRES) = 10.80
 TOTAL STREAM AREA(ACRES) = 10.80
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 36.85 ✓

 FLOW PROCESS FROM NODE 14.00 TO NODE 15.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<< ✓
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 279.00
 ELEVATION DATA: UPSTREAM(FEET) = 688.90 DOWNSTREAM(FEET) = 686.00

Tc = K* [(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.681
 * 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.838

SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL						
"11+ DWELLINGS/ACRE"	C	0.98	0.25	0.200	86	7.68

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.25
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
 SUBAREA RUNOFF(CFS) = 4.22
 TOTAL AREA(ACRES) = 0.98 PEAK FLOW RATE(CFS) = 4.22

 FLOW PROCESS FROM NODE 15.00 TO NODE 16.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

MAINLINE Tc(MIN.) = 7.68
 * 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.838

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL					
"11+ DWELLINGS/ACRE"	C	4.48	0.25	0.200	86

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.25
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
 SUBAREA AREA(ACRES) = 4.48 SUBAREA RUNOFF(CFS) = 19.30
 EFFECTIVE AREA(ACRES) = 5.46 AREA-AVERAGED Fm(INCH/HR) = 0.05
 AREA-AVERAGED Fp(INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.20
 TOTAL AREA(ACRES) = 5.5 PEAK FLOW RATE(CFS) = 23.53

 FLOW PROCESS FROM NODE 16.00 TO NODE 13.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 676.50 DOWNSTREAM(FEET) = 652.00
 FLOW LENGTH(FEET) = 140.00 MANNING'S N = 0.013
 ESTIMATED PIPE DIAMETER(INCH) INCREASED TO 18.000
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 9.8 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 23.78
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 23.53
 PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 7.78
 LONGEST FLOWPATH FROM NODE 14.00 TO NODE 13.00 = 419.00 FEET.

 FLOW PROCESS FROM NODE 13.00 TO NODE 13.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 7.78
 RAINFALL INTENSITY(INCH/HR) = 4.80
 AREA-AVERAGED Fm(INCH/HR) = 0.05
 AREA-AVERAGED Fp(INCH/HR) = 0.25
 AREA-AVERAGED Ap = 0.20
 EFFECTIVE STREAM AREA(ACRES) = 5.46
 TOTAL STREAM AREA(ACRES) = 5.46
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 23.53

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	32.53	7.89	4.764	0.25(0.05)	0.20	6.8	10.00
1	36.85	13.12	3.560	0.25(0.05)	0.20	10.8	6.00
2	23.53	7.78	4.803	0.25(0.05)	0.20	5.5	14.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	55.86	7.78	4.803	0.25 (0.05)	0.20	12.2	14.00
2	55.86	7.89	4.764	0.25 (0.05)	0.20	12.3	10.00
3	54.23	13.12	3.560	0.25 (0.05)	0.20	16.3	6.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 55.86 ✓ Tc (MIN.) = 7.89 ✓
 EFFECTIVE AREA (ACRES) = 12.29 AREA-AVERAGED Fm (INCH/HR) = 0.05
 AREA-AVERAGED Fp (INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.20
 TOTAL AREA (ACRES) = 16.3
 LONGEST FLOWPATH FROM NODE 6.00 TO NODE 13.00 = 1575.00 FEET.

 FLOW PROCESS FROM NODE 13.00 TO NODE 17.00 IS CODE = 31 ✓

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM (FEET) = 652.00 DOWNSTREAM (FEET) = 648.00
 FLOW LENGTH (FEET) = 280.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 33.0 INCH PIPE IS 25.9 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 11.17
 ESTIMATED PIPE DIAMETER (INCH) = 33.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 55.86
 PIPE TRAVEL TIME (MIN.) = 0.42 Tc (MIN.) = 8.31
 LONGEST FLOWPATH FROM NODE 6.00 TO NODE 17.00 = 1855.00 FEET.

 FLOW PROCESS FROM NODE 17.00 TO NODE 17.00 IS CODE = 1 ✓

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
 TIME OF CONCENTRATION (MIN.) = 8.31
 RAINFALL INTENSITY (INCH/HR) = 4.62
 AREA-AVERAGED Fm (INCH/HR) = 0.05
 AREA-AVERAGED Fp (INCH/HR) = 0.25
 AREA-AVERAGED Ap = 0.20
 EFFECTIVE STREAM AREA (ACRES) = 12.29
 TOTAL STREAM AREA (ACRES) = 16.26
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 55.86

 FLOW PROCESS FROM NODE 18.00 TO NODE 19.00 IS CODE = 21 ✓

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 216.00
 ELEVATION DATA: UPSTREAM (FEET) = 667.00 DOWNSTREAM (FEET) = 663.00

Tc = K * [(LENGTH** 3.00) / (ELEVATION CHANGE)]**0.20
 SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 5.796
 * 100 YEAR RAINFALL INTENSITY (INCH/HR) = 5.685
 SUBAREA Tc AND LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	D	0.37	0.20 ✓	0.100	91	5.80

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA RUNOFF (CFS) = 1.89
 TOTAL AREA (ACRES) = 0.37 PEAK FLOW RATE (CFS) = 1.89

FLOW PROCESS FROM NODE 19.00 TO NODE 20.00 IS CODE = 81 ✓

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 5.80
 * 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.685
 SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	D	1.35	0.20	0.100	91

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.20
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA AREA(ACRES) = 1.35 SUBAREA RUNOFF(CFS) = 6.88
 EFFECTIVE AREA(ACRES) = 1.72 AREA-AVERAGED Fm(INCH/HR) = 0.02
 AREA-AVERAGED Fp(INCH/HR) = 0.20 AREA-AVERAGED Ap = 0.10
 TOTAL AREA(ACRES) = 1.7 PEAK FLOW RATE(CFS) = 8.77

FLOW PROCESS FROM NODE 20.00 TO NODE 17.00 IS CODE = 31 ✓

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 654.50 DOWNSTREAM(FEET) = 648.00
 FLOW LENGTH(FEET) = 510.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.2 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 6.88
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 8.77
 PIPE TRAVEL TIME(MIN.) = 1.24 Tc(MIN.) = 7.03
 LONGEST FLOWPATH FROM NODE 18.00 TO NODE 17.00 = 726.00 FEET.

FLOW PROCESS FROM NODE 17.00 TO NODE 17.00 IS CODE = 1 ✓

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 7.03
 RAINFALL INTENSITY(INCH/HR) = 5.09
 AREA-AVERAGED Fm(INCH/HR) = 0.02
 AREA-AVERAGED Fp(INCH/HR) = 0.20
 AREA-AVERAGED Ap = 0.10
 EFFECTIVE STREAM AREA(ACRES) = 1.72
 TOTAL STREAM AREA(ACRES) = 1.72
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 8.77

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	55.86	8.20	4.661	0.25(0.05)	0.20	12.2	14.00
1	55.86	8.31	4.625	0.25(0.05)	0.20	12.3	10.00
1	54.23	13.54	3.497	0.25(0.05)	0.20	16.3	6.00
2	8.77	7.03	5.089	0.20(0.02)	0.10	1.7	18.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	61.14	7.03	5.089	0.25(0.05)	0.19	12.2	18.00
2	63.89	8.20	4.661	0.25(0.05)	0.19	13.9	14.00
3	63.83	8.31	4.625	0.25(0.05)	0.19	14.0	10.00
4	60.25	13.54	3.497	0.25(0.05)	0.19	18.0	6.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 63.89 ✓ Tc(MIN.) = 8.20 ✓
 EFFECTIVE AREA(ACRES) = 13.91 AREA-AVERAGED Fm(INCH/HR) = 0.05
 AREA-AVERAGED Fp(INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.19
 TOTAL AREA(ACRES) = 18.0
 LONGEST FLOWPATH FROM NODE 6.00 TO NODE 17.00 = 1855.00 FEET.

 FLOW PROCESS FROM NODE 17.00 TO NODE 21.00 IS CODE = 31 ✓

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW) <<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 648.00 DOWNSTREAM(FEET) = 637.70
 FLOW LENGTH(FEET) = 526.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 33.0 INCH PIPE IS 25.3 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 13.06
 ESTIMATED PIPE DIAMETER(INCH) = 33.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 63.89 ✓
 PIPE TRAVEL TIME(MIN.) = 0.67 Tc(MIN.) = 8.87 ✓
 LONGEST FLOWPATH FROM NODE 6.00 TO NODE 21.00 = 2381.00 FEET.

 FLOW PROCESS FROM NODE 21.00 TO NODE 21.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<< ✓

 FLOW PROCESS FROM NODE 22.00 TO NODE 23.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<< ✓
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 223.00
 ELEVATION DATA: UPSTREAM(FEET) = 691.00 DOWNSTREAM(FEET) = 687.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.297
 * 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.421
 SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL "11+ DWELLINGS/ACRE"	C	0.66 ✓	0.25	0.200	86	6.30

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.25
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
 SUBAREA RUNOFF(CFS) = 3.19
 TOTAL AREA(ACRES) = 0.66 PEAK FLOW RATE(CFS) = 3.19

 FLOW PROCESS FROM NODE 23.00 TO NODE 24.00 IS CODE = 81 ✓

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<< ✓

=====

MAINLINE Tc(MIN.) = 6.30
 * 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.421
 SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "11+ DWELLINGS/ACRE"	C	7.32 ✓	0.25	0.200	86

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.25
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
 SUBAREA AREA(ACRES) = 7.32 SUBAREA RUNOFF(CFS) = 35.39
 EFFECTIVE AREA(ACRES) = 7.98 AREA-AVERAGED Fm(INCH/HR) = 0.05
 AREA-AVERAGED Fp(INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.20
 TOTAL AREA(ACRES) = 8.0 PEAK FLOW RATE(CFS) = 38.58

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*****
FLOW PROCESS FROM NODE      24.00 TO NODE      25.00 IS CODE = 31 ✓
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 674.00 DOWNSTREAM(FEET) = 639.50
FLOW LENGTH(FEET) = 160.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.8 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 28.60
ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 38.58
PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 6.39
LONGEST FLOWPATH FROM NODE 22.00 TO NODE 25.00 = 383.00 FEET.

*****
FLOW PROCESS FROM NODE      25.00 TO NODE      25.00 IS CODE = 1 ✓
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 6.39
RAINFALL INTENSITY(INCH/HR) = 5.38
AREA-AVERAGED Fm(INCH/HR) = 0.05
AREA-AVERAGED Fp(INCH/HR) = 0.25
AREA-AVERAGED Ap = 0.20
EFFECTIVE STREAM AREA(ACRES) = 7.98
TOTAL STREAM AREA(ACRES) = 7.98 ✓
PEAK FLOW RATE(CFS) AT CONFLUENCE = 38.58 ✓

*****
FLOW PROCESS FROM NODE      26.00 TO NODE      41.00 IS CODE = 21 ✓
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 264.00
ELEVATION DATA: UPSTREAM(FEET) = 685.70 DOWNSTREAM(FEET) = 675.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.723
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.726
SUBAREA Tc AND LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/          SCS SOIL          Fp          Ap          SCS          Tc
LAND USE                   GROUP   (ACRES)   (INCH/HR)   (DECIMAL)   CN   (MIN.)
RESIDENTIAL
"11+ DWELLINGS/ACRE"      C         0.44 ✓    0.25        0.200        86    5.72
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.25
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA RUNOFF(CFS) = 2.25
TOTAL AREA(ACRES) = 0.44 PEAK FLOW RATE(CFS) = 2.25

*****
FLOW PROCESS FROM NODE      41.00 TO NODE      25.00 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 675.00 DOWNSTREAM ELEVATION(FEET) = 650.00
STREET LENGTH(FEET) = 760.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020

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Manning's FRICTION FACTOR for Streetflow Section(curbed-to-curb) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.48
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.34
HALFSTREET FLOOD WIDTH(FEET) = 10.81
AVERAGE FLOW VELOCITY(FEET/SEC.) = 4.25
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.46
STREET FLOW TRAVEL TIME(MIN.) = 2.98 Tc(MIN.) = 8.70
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.505
SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "11+ DWELLINGS/ACRE"	C	1.60	0.25	0.200	86

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.25
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA AREA(ACRES) = 1.60 SUBAREA RUNOFF(CFS) = 6.41
EFFECTIVE AREA(ACRES) = 2.04 AREA-AVERAGED Fm(INCH/HR) = 0.05
AREA-AVERAGED Fp(INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.20
TOTAL AREA(ACRES) = 2.0 PEAK FLOW RATE(CFS) = 8.18

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.38 HALFSTREET FLOOD WIDTH(FEET) = 12.79
FLOW VELOCITY(FEET/SEC.) = 4.66 DEPTH*VELOCITY(FT*FT/SEC.) = 1.78
LONGEST FLOWPATH FROM NODE 26.00 TO NODE 25.00 = 1024.00 FEET.

FLOW PROCESS FROM NODE 25.00 TO NODE 25.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 8.70
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.505
SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "11+ DWELLINGS/ACRE"	C	2.23	0.25	0.200	86

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.25
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA AREA(ACRES) = 2.23 SUBAREA RUNOFF(CFS) = 8.94
EFFECTIVE AREA(ACRES) = 4.27 AREA-AVERAGED Fm(INCH/HR) = 0.05
AREA-AVERAGED Fp(INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.20
TOTAL AREA(ACRES) = 4.3 PEAK FLOW RATE(CFS) = 17.12

FLOW PROCESS FROM NODE 25.00 TO NODE 25.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 8.70
RAINFALL INTENSITY(INCH/HR) = 4.50
AREA-AVERAGED Fm(INCH/HR) = 0.05
AREA-AVERAGED Fp(INCH/HR) = 0.25
AREA-AVERAGED Ap = 0.20
EFFECTIVE STREAM AREA(ACRES) = 4.27
TOTAL STREAM AREA(ACRES) = 4.27
PEAK FLOW RATE(CFS) AT CONFLUENCE = 17.12

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	38.58	6.39	5.376	0.25 (0.05)	0.20	8.0	22.00
2	17.12	8.70	4.505	0.25 (0.05)	0.20	4.3	26.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	53.61	6.39	5.376	0.25 (0.05)	0.20	11.1	22.00
2	49.39	8.70	4.505	0.25 (0.05)	0.20	12.2	26.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 53.61 Tc(MIN.) = 6.39
 EFFECTIVE AREA(ACRES) = 11.12 AREA-AVERAGED Fm(INCH/HR) = 0.05
 AREA-AVERAGED Fp(INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.20
 TOTAL AREA(ACRES) = 12.2
 LONGEST FLOWPATH FROM NODE 26.00 TO NODE 25.00 = 1024.00 FEET.

 FLOW PROCESS FROM NODE 25.00 TO NODE 21.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 639.50 DOWNSTREAM(FEET) = 637.70
 FLOW LENGTH(FEET) = 240.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 39.0 INCH PIPE IS 26.7 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 8.85
 ESTIMATED PIPE DIAMETER(INCH) = 39.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 53.61
 PIPE TRAVEL TIME(MIN.) = 0.45 Tc(MIN.) = 6.84
 LONGEST FLOWPATH FROM NODE 26.00 TO NODE 21.00 = 1264.00 FEET.

 FLOW PROCESS FROM NODE 21.00 TO NODE 21.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

** MAIN STREAM CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	53.61	6.84	5.170	0.25 (0.05)	0.20	11.1	22.00
2	49.39	9.17	4.372	0.25 (0.05)	0.20	12.2	26.00

LONGEST FLOWPATH FROM NODE 26.00 TO NODE 21.00 = 1264.00 FEET.

** MEMORY BANK # 1 CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	61.14	7.71	4.829	0.25 (0.05)	0.19	12.2	18.00
2	63.89	8.87	4.455	0.25 (0.05)	0.19	13.9	14.00
3	63.83	8.98	4.424	0.25 (0.05)	0.19	14.0	10.00
4	60.25	14.21	3.401	0.25 (0.05)	0.19	18.0	6.00

LONGEST FLOWPATH FROM NODE 6.00 TO NODE 21.00 = 2381.00 FEET.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	111.75	6.84	5.170	0.25 (0.05)	0.19	21.9	22.00
2	113.18	7.71	4.829	0.25 (0.05)	0.19	23.7	18.00
3	113.82	8.87	4.455	0.25 (0.05)	0.19	26.0	14.00
4	113.55	8.98	4.424	0.25 (0.05)	0.19	26.2	10.00
5	113.08	9.17	4.372	0.25 (0.05)	0.19	26.4	26.00
6	98.54	14.21	3.401	0.25 (0.05)	0.19	30.2	6.00

TOTAL AREA(ACRES) = 30.2

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 113.82 Tc(MIN.) = 8.868
 EFFECTIVE AREA(ACRES) = 26.01 AREA-AVERAGED Fm(INCH/HR) = 0.05
 AREA-AVERAGED Fp(INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.19

```

TOTAL AREA(ACRES) = 30.2
LONGEST FLOWPATH FROM NODE 6.00 TO NODE 21.00 = 2381.00 FEET.
*****
FLOW PROCESS FROM NODE 21.00 TO NODE 21.00 IS CODE = 12
-----
>>>>CLEAR MEMORY BANK # 1 <<<<
=====
*****
FLOW PROCESS FROM NODE 21.00 TO NODE 26.00 IS CODE = 31
-----
>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<
=====
ELEVATION DATA: UPSTREAM(FEET) = 637.70 DOWNSTREAM(FEET) = 636.50
FLOW LENGTH(FEET) = 160.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 48.0 INCH PIPE IS 39.0 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.40
ESTIMATED PIPE DIAMETER(INCH) = 48.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 113.82
PIPE TRAVEL TIME(MIN.) = 0.26 Tc(MIN.) = 9.12
LONGEST FLOWPATH FROM NODE 6.00 TO NODE 26.00 = 2541.00 FEET.
*****
FLOW PROCESS FROM NODE 26.00 TO NODE 26.00 IS CODE = 1
-----
>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<
=====
TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION(MIN.) = 9.12
RAINFALL INTENSITY(INCH/HR) = 4.38
AREA-AVERAGED Fm(INCH/HR) = 0.05
AREA-AVERAGED Fp(INCH/HR) = 0.25
AREA-AVERAGED Ap = 0.19
EFFECTIVE STREAM AREA(ACRES) = 26.01
TOTAL STREAM AREA(ACRES) = 30.23
PEAK FLOW RATE(CFS) AT CONFLUENCE = 113.82
*****
FLOW PROCESS FROM NODE 27.00 TO NODE 28.00 IS CODE = 21
-----
>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<
=====
INITIAL SUBAREA FLOW-LENGTH(FEET) = 225.00
ELEVATION DATA: UPSTREAM(FEET) = 658.30 DOWNSTREAM(FEET) = 657.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 7.926
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.752
SUBAREA Tc AND LOSS RATE DATA(AMC III):
DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS Tc
LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN (MIN.)
RESIDENTIAL
"11+ DWELLINGS/ACRE" C 0.49 0.25 0.200 86 7.93
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.25
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
SUBAREA RUNOFF(CFS) = 2.07
TOTAL AREA(ACRES) = 0.49 PEAK FLOW RATE(CFS) = 2.07
*****
FLOW PROCESS FROM NODE 28.00 TO NODE 26.00 IS CODE = 62
-----
>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<
=====
UPSTREAM ELEVATION(FEET) = 657.00 DOWNSTREAM ELEVATION(FEET) = 642.00

```

STREET LENGTH(FEET) = 1020.00 CURB HEIGHT(INCHES) = 6.0
 STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00
 INSIDE STREET CROSSFALL(DECIMAL) = 0.020
 OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
 STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
 Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
 Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 11.07

STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:

STREET FLOW DEPTH(FEET) = 0.47
 HALFSTREET FLOOD WIDTH(FEET) = 16.96
 AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.70
 PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.72
 STREET FLOW TRAVEL TIME(MIN.) = 4.60 Tc(MIN.) = 12.52
 * 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.656

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "11+ DWELLINGS/ACRE"	C	5.50	0.25	0.200	86
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.25					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200					
SUBAREA AREA(ACRES) = 5.50		SUBAREA RUNOFF(CFS) = 17.85			
EFFECTIVE AREA(ACRES) = 5.99		AREA-AVERAGED Fm(INCH/HR) = 0.05			
AREA-AVERAGED Fp(INCH/HR) = 0.25		AREA-AVERAGED Ap = 0.20			
TOTAL AREA(ACRES) = 6.0		PEAK FLOW RATE(CFS) = 19.44			

END OF SUBAREA STREET FLOW HYDRAULICS:

DEPTH(FEET) = 0.49 HALFSTREET FLOOD WIDTH(FEET) = 18.00
 FLOW VELOCITY(FEET/SEC.) = 3.85 DEPTH*VELOCITY(FT*FT/SEC.) = 1.87
 LONGEST FLOWPATH FROM NODE 27.00 TO NODE 26.00 = 1245.00 FEET.

 FLOW PROCESS FROM NODE 26.00 TO NODE 26.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 12.52
 RAINFALL INTENSITY(INCH/HR) = 3.66
 AREA-AVERAGED Fm(INCH/HR) = 0.05
 AREA-AVERAGED Fp(INCH/HR) = 0.25
 AREA-AVERAGED Ap = 0.20
 EFFECTIVE STREAM AREA(ACRES) = 5.99
 TOTAL STREAM AREA(ACRES) = 5.99
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 19.44

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	111.75	7.10	5.062	0.25(0.05)	0.19	21.9	22.00
1	113.18	7.96	4.739	0.25(0.05)	0.19	23.7	18.00
1	113.82	9.12	4.383	0.25(0.05)	0.19	26.0	14.00
1	113.55	9.24	4.353	0.25(0.05)	0.19	26.2	10.00
1	113.08	9.42	4.303	0.25(0.05)	0.19	26.4	26.00
1	98.54	14.47	3.365	0.25(0.05)	0.19	30.2	6.00
2	19.44	12.52	3.656	0.25(0.05)	0.20	6.0	27.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	127.07	7.10	5.062	0.25 (0.05)	0.19	25.3	22.00
2	129.25	7.96	4.739	0.25 (0.05)	0.19	27.5	18.00
3	130.84	9.12	4.383	0.25 (0.05)	0.19	30.4	14.00
4	130.66	9.24	4.353	0.25 (0.05)	0.19	30.6	10.00
5	130.34	9.42	4.303	0.25 (0.05)	0.19	30.9	26.00
6	123.59	12.52	3.656	0.25 (0.05)	0.20	34.7	27.00
7	116.41	14.47	3.365	0.25 (0.05)	0.20	36.2	6.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 130.84 ✓ Tc(MIN.) = 9.12 ✓
 EFFECTIVE AREA(ACRES) = 30.38 AREA-AVERAGED Fm(INCH/HR) = 0.05
 AREA-AVERAGED Fp(INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.19
 TOTAL AREA(ACRES) = 36.2
 LONGEST FLOWPATH FROM NODE 6.00 TO NODE 26.00 = 2541.00 FEET.

 FLOW PROCESS FROM NODE 26.00 TO NODE 29.00 IS CODE = 31 ✓

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 636.50 DOWNSTREAM(FEET) = 636.00
 FLOW LENGTH(FEET) = 40.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 48.0 INCH PIPE IS 35.1 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 13.30
 ESTIMATED PIPE DIAMETER(INCH) = 48.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 130.84
 PIPE TRAVEL TIME(MIN.) = 0.05 Tc(MIN.) = 9.17
 LONGEST FLOWPATH FROM NODE 6.00 TO NODE 29.00 = 2581.00 FEET.

 FLOW PROCESS FROM NODE 29.00 TO NODE 29.00 IS CODE = 1 ✓

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
 TIME OF CONCENTRATION(MIN.) = 9.17
 RAINFALL INTENSITY(INCH/HR) = 4.37
 AREA-AVERAGED Fm(INCH/HR) = 0.05
 AREA-AVERAGED Fp(INCH/HR) = 0.25
 AREA-AVERAGED Ap = 0.19
 EFFECTIVE STREAM AREA(ACRES) = 30.38
 TOTAL STREAM AREA(ACRES) = 36.22
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 130.84 ✓

 FLOW PROCESS FROM NODE 30.00 TO NODE 31.00 IS CODE = 21 ✓

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 190.00
 ELEVATION DATA: UPSTREAM(FEET) = 672.00 DOWNSTREAM(FEET) = 670.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
 SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.570
 * 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.291
 SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL "11+ DWELLINGS/ACRE"	C	0.40 ✓	0.25	0.200	86	6.57

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.25
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200

SUBAREA RUNOFF(CFS) = 1.89
TOTAL AREA(ACRES) = 0.40 PEAK FLOW RATE(CFS) = 1.89

FLOW PROCESS FROM NODE 31.00 TO NODE 32.00 IS CODE = 62 ✓

>>>>COMPUTE STREET FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>(STREET TABLE SECTION # 1 USED)<<<<<

=====

UPSTREAM ELEVATION(FEET) = 670.00 DOWNSTREAM ELEVATION(FEET) = 652.00
STREET LENGTH(FEET) = 1770.00 CURB HEIGHT(INCHES) = 6.0
STREET HALFWIDTH(FEET) = 18.00

DISTANCE FROM CROWN TO CROSSFALL GRADEBREAK(FEET) = 13.00
INSIDE STREET CROSSFALL(DECIMAL) = 0.020
OUTSIDE STREET CROSSFALL(DECIMAL) = 0.020

SPECIFIED NUMBER OF HALFSTREETS CARRYING RUNOFF = 1
STREET PARKWAY CROSSFALL(DECIMAL) = 0.020
Manning's FRICTION FACTOR for Streetflow Section(curbs-to-curbs) = 0.0150
Manning's FRICTION FACTOR for Back-of-Walk Flow Section = 0.0200

**TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 15.75
STREET FLOW SPLITS OVER STREET-CROWN
FULL DEPTH(FEET) = 0.49 FLOOD WIDTH(FEET) = 18.00
FULL HALF-STREET VELOCITY(FEET/SEC.) = 3.20
SPLIT DEPTH(FEET) = 0.39 SPLIT FLOOD WIDTH(FEET) = 13.30
SPLIT FLOW(CFS) = 5.00 SPLIT VELOCITY(FEET/SEC.) = 2.65
STREETFLOW MODEL RESULTS USING ESTIMATED FLOW:
STREET FLOW DEPTH(FEET) = 0.49
HALFSTREET FLOOD WIDTH(FEET) = 18.00
AVERAGE FLOW VELOCITY(FEET/SEC.) = 3.20
PRODUCT OF DEPTH&VELOCITY(FT*FT/SEC.) = 1.56
STREET FLOW TRAVEL TIME(MIN.) = 9.22 Tc(MIN.) = 15.79
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 3.201
SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL "11+ DWELLINGS/ACRE"	C	9.60 ✓	0.25	0.200	86
SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.25					
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200					
SUBAREA AREA(ACRES) = 9.60 SUBAREA RUNOFF(CFS) = 27.23					
EFFECTIVE AREA(ACRES) = 10.00 AREA-AVERAGED Fm(INCH/HR) = 0.05					
AREA-AVERAGED Fp(INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.20					
TOTAL AREA(ACRES) = 10.0 PEAK FLOW RATE(CFS) = 28.36 ✓					

END OF SUBAREA STREET FLOW HYDRAULICS:
DEPTH(FEET) = 0.52 HALFSTREET FLOOD WIDTH(FEET) = 18.99
FLOW VELOCITY(FEET/SEC.) = 3.57 DEPTH*VELOCITY(FT*FT/SEC.) = 1.86
*NOTE: INITIAL SUBAREA NOMOGRAPH WITH SUBAREA PARAMETERS,
AND L = 1770.0 FT WITH ELEVATION-DROP = 18.0 FT, IS 26.9 CFS,
WHICH EXCEEDS THE TOP-OF-CURB STREET CAPACITY AT NODE 32.00
LONGEST FLOWPATH FROM NODE 30.00 TO NODE 32.00 = 1960.00 FEET.

FLOW PROCESS FROM NODE 32.00 TO NODE 29.00 IS CODE = 31 ✓

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 644.00 DOWNSTREAM(FEET) = 636.00
FLOW LENGTH(FEET) = 450.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 27.0 INCH PIPE IS 17.4 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 10.49
ESTIMATED PIPE DIAMETER(INCH) = 27.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 28.36
PIPE TRAVEL TIME(MIN.) = 0.71 Tc(MIN.) = 16.50
LONGEST FLOWPATH FROM NODE 30.00 TO NODE 29.00 = 2410.00 FEET.

 FLOW PROCESS FROM NODE 29.00 TO NODE 29.00 IS CODE = 1 ✓

 >>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<
 =====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION (MIN.) = 16.50
 RAINFALL INTENSITY (INCH/HR) = 3.12
 AREA-AVERAGED Fm (INCH/HR) = 0.05
 AREA-AVERAGED Fp (INCH/HR) = 0.25
 AREA-AVERAGED Ap = 0.20
 EFFECTIVE STREAM AREA (ACRES) = 10.00
 TOTAL STREAM AREA (ACRES) = 10.00 ✓
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 28.36 ✓

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	127.07	7.15	5.041	0.25 (0.05)	0.19	25.3	22.00
1	129.25	8.01	4.722	0.25 (0.05)	0.19	27.5	18.00
1	130.84	9.17	4.370	0.25 (0.05)	0.19	30.4	14.00
1	130.66	9.29	4.339	0.25 (0.05)	0.19	30.6	10.00
1	130.34	9.47	4.290	0.25 (0.05)	0.19	30.9	26.00
1	123.59	12.57	3.648	0.25 (0.05)	0.20	34.7	27.00
1	116.41	14.52	3.359	0.25 (0.05)	0.20	36.2	6.00
2	28.36	16.50	3.121	0.25 (0.05)	0.20	10.0	30.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp (Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	147.03	7.15	5.041	0.25 (0.05)	0.19	29.7	22.00
2	150.20	8.01	4.722	0.25 (0.05)	0.19	32.4	18.00
3	153.01	9.17	4.370	0.25 (0.05)	0.20	35.9	14.00
4	152.95	9.29	4.339	0.25 (0.05)	0.20	36.2	10.00
5	152.81	9.47	4.290	0.25 (0.05)	0.20	36.6	26.00
6	148.90	12.57	3.648	0.25 (0.05)	0.20	42.4	27.00
7	143.30	14.52	3.359	0.25 (0.05)	0.20	45.0	6.00
8	136.43	16.50	3.121	0.25 (0.05)	0.20	46.2	30.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 153.01 ✓ Tc (MIN.) = 9.17
 EFFECTIVE AREA (ACRES) = 35.94 AREA-AVERAGED Fm (INCH/HR) = 0.05
 AREA-AVERAGED Fp (INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.20
 TOTAL AREA (ACRES) = 46.2
 LONGEST FLOWPATH FROM NODE 6.00 TO NODE 29.00 = 2581.00 FEET.

 FLOW PROCESS FROM NODE 29.00 TO NODE 42.00 IS CODE = 31

 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<< ✓
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
 =====

ELEVATION DATA: UPSTREAM (FEET) = 636.00 DOWNSTREAM (FEET) = 610.00
 FLOW LENGTH (FEET) = 400.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 36.0 INCH PIPE IS 28.8 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 25.28
 ESTIMATED PIPE DIAMETER (INCH) = 36.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 153.01
 PIPE TRAVEL TIME (MIN.) = 0.26 Tc (MIN.) = 9.44
 LONGEST FLOWPATH FROM NODE 6.00 TO NODE 42.00 = 2981.00 FEET.

FLOW PROCESS FROM NODE 42.00 TO NODE 42.00 IS CODE = 81

AREA C3

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc (MIN.) = 9.44
 * 100 YEAR RAINFALL INTENSITY (INCH/HR) = 4.299
 SUBAREA LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL GOOD COVER "CHAPARRAL, BROADLEAF"	C	1.18	0.25	1.000	88

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.25
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
 SUBAREA AREA (ACRES) = 1.18 SUBAREA RUNOFF (CFS) = 4.30
 EFFECTIVE AREA (ACRES) = 37.12 AREA-AVERAGED Fm (INCH/HR) = 0.05
 AREA-AVERAGED Fp (INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.22
 TOTAL AREA (ACRES) = 47.4 PEAK FLOW RATE (CFS) = 153.01
 NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

FLOW PROCESS FROM NODE 42.00 TO NODE 33.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM (FEET) = 610.00 DOWNSTREAM (FEET) = 608.50
 FLOW LENGTH (FEET) = 270.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 57.0 INCH PIPE IS 45.7 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 10.04
 ESTIMATED PIPE DIAMETER (INCH) = 57.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 153.01
 PIPE TRAVEL TIME (MIN.) = 0.45 Tc (MIN.) = 9.89
 LONGEST FLOWPATH FROM NODE 6.00 TO NODE 33.00 = 3251.00 FEET.

FLOW PROCESS FROM NODE 33.00 TO NODE 33.00 IS CODE = 10

>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 2 <<<<<

FLOW PROCESS FROM NODE 34.00 TO NODE 35.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH (FEET) = 254.00
 ELEVATION DATA: UPSTREAM (FEET) = 658.70 DOWNSTREAM (FEET) = 656.00

$Tc = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
 SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 7.365
 * 100 YEAR RAINFALL INTENSITY (INCH/HR) = 4.956
 SUBAREA Tc AND LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL "11+ DWELLINGS/ACRE"	C	1.34	0.25	0.200	86	7.36

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.25
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
 SUBAREA RUNOFF (CFS) = 5.92
 TOTAL AREA (ACRES) = 1.34 PEAK FLOW RATE (CFS) = 5.92

FLOW PROCESS FROM NODE 35.00 TO NODE 36.00 IS CODE = 81 ✓

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

MAINLINE Tc(MIN.) = 7.36

* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 4.956

SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
RESIDENTIAL					
"11+ DWELLINGS/ACRE"	C	2.58 ✓	0.25	0.200	86

RESIDENTIAL

"11+ DWELLINGS/ACRE"

C

2.58 ✓

0.25

0.200

86

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.25

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200

SUBAREA AREA(ACRES) = 2.58 SUBAREA RUNOFF(CFS) = 11.39

EFFECTIVE AREA(ACRES) = 3.92 AREA-AVERAGED Fm(INCH/HR) = 0.05

AREA-AVERAGED Fp(INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.20

TOTAL AREA(ACRES) = 3.9 PEAK FLOW RATE(CFS) = 17.31 ✓

FLOW PROCESS FROM NODE 36.00 TO NODE 37.00 IS CODE = 31 ✓

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<

>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 645.30 DOWNSTREAM(FEET) = 638.90

FLOW LENGTH(FEET) = 140.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.6 INCHES

PIPE-FLOW VELOCITY(FEET/SEC.) = 13.12

ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1

PIPE-FLOW(CFS) = 17.31

PIPE TRAVEL TIME(MIN.) = 0.18 Tc(MIN.) = 7.54

LONGEST FLOWPATH FROM NODE 34.00 TO NODE 37.00 = 394.00 FEET.

FLOW PROCESS FROM NODE 37.00 TO NODE 37.00 IS CODE = 1 ✓

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<

TOTAL NUMBER OF STREAMS = 2

CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:

TIME OF CONCENTRATION(MIN.) = 7.54

RAINFALL INTENSITY(INCH/HR) = 4.89

AREA-AVERAGED Fm(INCH/HR) = 0.05

AREA-AVERAGED Fp(INCH/HR) = 0.25

AREA-AVERAGED Ap = 0.20

EFFECTIVE STREAM AREA(ACRES) = 3.92

TOTAL STREAM AREA(ACRES) = 3.92

PEAK FLOW RATE(CFS) AT CONFLUENCE = 17.31 ✓

FLOW PROCESS FROM NODE 38.00 TO NODE 39.00 IS CODE = 21 ✓

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<

>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 132.00

ELEVATION DATA: UPSTREAM(FEET) = 651.30 DOWNSTREAM(FEET) = 650.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 5.756

* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.708

SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
RESIDENTIAL						
"11+ DWELLINGS/ACRE"	C	1.08	0.25	0.200	86	5.76

RESIDENTIAL

"11+ DWELLINGS/ACRE"

C

1.08

0.25

0.200

86

5.76

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.25

SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200

SUBAREA RUNOFF(CFS) = 5.50
 TOTAL AREA(ACRES) = 1.08 PEAK FLOW RATE(CFS) = 5.50

 FLOW PROCESS FROM NODE 39.00 TO NODE 37.00 IS CODE = 81

AREA A19

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

MAINLINE Tc(MIN.) = 5.76
 * 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.708
 SUBAREA LOSS RATE DATA(AMC III):
 DEVELOPMENT TYPE/ SCS SOIL AREA Fp Ap SCS
 LAND USE GROUP (ACRES) (INCH/HR) (DECIMAL) CN
 RESIDENTIAL
 "11+ DWELLINGS/ACRE" C 3.24 0.25 0.200 86
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.25
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.200
 SUBAREA AREA(ACRES) = 3.24 SUBAREA RUNOFF(CFS) = 16.50
 EFFECTIVE AREA(ACRES) = 4.32 AREA-AVERAGED Fm(INCH/HR) = 0.05
 AREA-AVERAGED Fp(INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.20
 TOTAL AREA(ACRES) = 4.3 PEAK FLOW RATE(CFS) = 22.00

 FLOW PROCESS FROM NODE 37.00 TO NODE 37.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
 >>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
 TIME OF CONCENTRATION(MIN.) = 5.76
 RAINFALL INTENSITY(INCH/HR) = 5.71
 AREA-AVERAGED Fm(INCH/HR) = 0.05
 AREA-AVERAGED Fp(INCH/HR) = 0.25
 AREA-AVERAGED Ap = 0.20
 EFFECTIVE STREAM AREA(ACRES) = 4.32
 TOTAL STREAM AREA(ACRES) = 4.32
 PEAK FLOW RATE(CFS) AT CONFLUENCE = 22.00

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	17.31	7.54	4.889	0.25(0.05)	0.20	3.9	34.00
2	22.00	5.76	5.708	0.25(0.05)	0.20	4.3	38.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
 CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	37.44	5.76	5.708	0.25(0.05)	0.20	7.3	38.00
2	36.12	7.54	4.889	0.25(0.05)	0.20	8.2	34.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 37.44 Tc(MIN.) = 5.76
 EFFECTIVE AREA(ACRES) = 7.31 AREA-AVERAGED Fm(INCH/HR) = 0.05
 AREA-AVERAGED Fp(INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.20
 TOTAL AREA(ACRES) = 8.2
 LONGEST FLOWPATH FROM NODE 34.00 TO NODE 37.00 = 394.00 FEET.

 FLOW PROCESS FROM NODE 37.00 TO NODE 33.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 638.90 DOWNSTREAM(FEET) = 608.50
 FLOW LENGTH(FEET) = 146.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.7 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 28.06
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 37.44
 PIPE TRAVEL TIME(MIN.) = 0.09 Tc(MIN.) = 5.84
 LONGEST FLOWPATH FROM NODE 34.00 TO NODE 33.00 = 540.00 FEET.

 FLOW PROCESS FROM NODE 33.00 TO NODE 33.00 IS CODE = 11 ✓

 >>>>CONFLUENCE MEMORY BANK # 2 WITH THE MAIN-STREAM MEMORY<<<<<
 =====

** MAIN STREAM CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	37.44	5.84	5.659	0.25 (0.05)	0.20	7.3	38.00
2	36.12	7.63	4.856	0.25 (0.05)	0.20	8.2	34.00

LONGEST FLOWPATH FROM NODE 34.00 TO NODE 33.00 = 540.00 FEET.

** MEMORY BANK # 2 CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	147.03	7.86	4.774	0.25 (0.06)	0.23	30.8	22.00
2	150.20	8.73	4.497	0.25 (0.06)	0.22	33.6	18.00
3	153.01	9.89	4.186	0.25 (0.05)	0.22	37.1	14.00
4	152.95	10.00	4.159	0.25 (0.05)	0.22	37.4	10.00
5	152.81	10.19	4.115	0.25 (0.05)	0.22	37.8	26.00
6	148.90	13.29	3.534	0.25 (0.05)	0.22	43.5	27.00
7	143.30	15.24	3.267	0.25 (0.05)	0.22	46.2	6.00
8	136.43	17.22	3.046	0.25 (0.05)	0.22	47.4	30.00

LONGEST FLOWPATH FROM NODE 6.00 TO NODE 33.00 = 3251.00 FEET.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	167.21	5.84	5.659	0.25 (0.05)	0.22	30.2	38.00
2	181.31	7.63	4.856	0.25 (0.05)	0.22	38.2	34.00
3	182.53	7.86	4.774	0.25 (0.05)	0.22	39.1	22.00
4	183.62	8.73	4.497	0.25 (0.05)	0.22	41.8	18.00
5	184.10	9.89	4.186	0.25 (0.05)	0.22	45.4	14.00
6	183.83	10.00	4.159	0.25 (0.05)	0.22	45.6	10.00
7	183.37	10.19	4.115	0.25 (0.05)	0.22	46.1	26.00
8	175.09	13.29	3.534	0.25 (0.05)	0.21	51.8	27.00
9	167.47	15.24	3.267	0.25 (0.05)	0.21	54.4	6.00
10	158.94	17.22	3.046	0.25 (0.05)	0.21	55.6	30.00

TOTAL AREA(ACRES) = 55.6

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 184.10 ✓ Tc(MIN.) = 9.887 ✓
 EFFECTIVE AREA(ACRES) = 45.36 AREA-AVERAGED Fm(INCH/HR) = 0.05
 AREA-AVERAGED Fp(INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.22
 TOTAL AREA(ACRES) = 55.6
 LONGEST FLOWPATH FROM NODE 6.00 TO NODE 33.00 = 3251.00 FEET.

 FLOW PROCESS FROM NODE 33.00 TO NODE 33.00 IS CODE = 12 ✓

 >>>>CLEAR MEMORY BANK # 2 <<<<<
 =====

 FLOW PROCESS FROM NODE 33.00 TO NODE 40.00 IS CODE = 31 ✓

 >>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<
 =====

ELEVATION DATA: UPSTREAM(FEET) = 608.50 DOWNSTREAM(FEET) = 590.00
 FLOW LENGTH(FEET) = 70.00 MANNING'S N = 0.013

DEPTH OF FLOW IN 30.0 INCH PIPE IS 23.3 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 45.06
 ESTIMATED PIPE DIAMETER (INCH) = 30.00 NUMBER OF PIPES = 1
 PIPE-FLOW (CFS) = 184.10
 PIPE TRAVEL TIME (MIN.) = 0.03 Tc (MIN.) = 9.91
 LONGEST FLOWPATH FROM NODE 6.00 TO NODE 40.00 = 3321.00 FEET.

 FLOW PROCESS FROM NODE 40.00 TO NODE 40.00 IS CODE = 1 ✓

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
 CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
 TIME OF CONCENTRATION (MIN.) = 9.91
 RAINFALL INTENSITY (INCH/HR) = 4.18
 AREA-AVERAGED Fm (INCH/HR) = 0.05
 AREA-AVERAGED Fp (INCH/HR) = 0.25
 AREA-AVERAGED Ap = 0.22
 EFFECTIVE STREAM AREA (ACRES) = 45.36
 TOTAL STREAM AREA (ACRES) = 55.64 ✓
 PEAK FLOW RATE (CFS) AT CONFLUENCE = 184.10 ✓

 FLOW PROCESS FROM NODE 43.00 TO NODE 44.00 IS CODE = 21 ✓ AREA C5

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
 >>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 365.00
 ELEVATION DATA: UPSTREAM (FEET) = 645.00 DOWNSTREAM (FEET) = 608.00

Tc = K * [(LENGTH** 3.00) / (ELEVATION CHANGE)] ** 0.20
 SUBAREA ANALYSIS USED MINIMUM Tc (MIN.) = 5.089
 * 100 YEAR RAINFALL INTENSITY (INCH/HR) = 6.125
 SUBAREA Tc AND LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	C	3.24 ✓	0.25	0.100	86	5.09

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.25
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA RUNOFF (CFS) = 17.79
 TOTAL AREA (ACRES) = 3.24 PEAK FLOW RATE (CFS) = 17.79

 FLOW PROCESS FROM NODE 44.00 TO NODE 40.00 IS CODE = 81 ✓ AREA C6

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc (MIN.) = 5.09
 * 100 YEAR RAINFALL INTENSITY (INCH/HR) = 6.125
 SUBAREA LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL GOOD COVER "GRASS"	C	4.48 ✓	0.25	1.000	90

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp (INCH/HR) = 0.25
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
 SUBAREA AREA (ACRES) = 4.48 SUBAREA RUNOFF (CFS) = 23.69
 EFFECTIVE AREA (ACRES) = 7.72 AREA-AVERAGED Fm (INCH/HR) = 0.16
 AREA-AVERAGED Fp (INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.62
 TOTAL AREA (ACRES) = 7.7 PEAK FLOW RATE (CFS) = 41.48

FLOW PROCESS FROM NODE 40.00 TO NODE 40.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<
>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 5.09
RAINFALL INTENSITY(INCH/HR) = 6.13
AREA-AVERAGED Fm(INCH/HR) = 0.16
AREA-AVERAGED Fp(INCH/HR) = 0.25
AREA-AVERAGED Ap = 0.62
EFFECTIVE STREAM AREA(ACRES) = 7.72
TOTAL STREAM AREA(ACRES) = 7.72
PEAK FLOW RATE(CFS) AT CONFLUENCE = 41.48

** CONFLUENCE DATA **

Table with 9 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp(Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. Contains 15 rows of data.

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

Table with 9 columns: STREAM NUMBER, Q (CFS), Tc (MIN.), Intensity (INCH/HR), Fp(Fm) (INCH/HR), Ap, Ae (ACRES), HEADWATER NODE. Contains 11 rows of data.

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 214.56 Tc(MIN.) = 7.89
EFFECTIVE AREA(ACRES) = 46.79 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.29
TOTAL AREA(ACRES) = 63.4
LONGEST FLOWPATH FROM NODE 6.00 TO NODE 40.00 = 3321.00 FEET.

END OF STUDY SUMMARY:

TOTAL AREA(ACRES) = 63.4 TC(MIN.) = 7.89
EFFECTIVE AREA(ACRES) = 46.79 AREA-AVERAGED Fm(INCH/HR) = 0.07
AREA-AVERAGED Fp(INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.287
PEAK FLOW RATE(CFS) = 214.56

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	198.93	5.09	6.125	0.25 (0.08)	0.31	33.9	43.00
2	205.35	5.87	5.645	0.25 (0.08)	0.30	37.9	38.00
3	213.91	7.66	4.847	0.25 (0.07)	0.29	45.9	34.00
4	214.56	7.89	4.765	0.25 (0.07)	0.29	46.8	22.00
5	213.73	8.75	4.489	0.25 (0.07)	0.28	49.5	18.00
6	212.06	9.91	4.180	0.25 (0.07)	0.28	53.1	14.00
7	211.61	10.02	4.153	0.25 (0.07)	0.28	53.4	10.00
8	210.84	10.21	4.109	0.25 (0.07)	0.27	53.8	26.00
9	198.53	13.31	3.530	0.25 (0.07)	0.27	59.5	27.00
10	189.07	15.26	3.264	0.25 (0.07)	0.26	62.2	6.00
11	179.00	17.25	3.043	0.25 (0.07)	0.26	63.4	30.00

=====
 END OF RATIONAL METHOD ANALYSIS
 =====

PROPOSED CIVIC CENTER

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
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Ver. 13.5 Release Date: 02/06/2007 License ID 1355

Analysis prepared by:

Fuscoe Engineering
16795 Von Karman Suite 100 Irvine Ca 92606

***** DESCRIPTION OF STUDY *****
* I.R.W.D. - LAKE FOREST SITE *
* PROPOSED 100 YEAR HYDROLOGY STUDY CIVIC CENTER/EXISTING TANK *
* DEVELOPER: LEWIS OPERATING CORP. *

FILE NAME: IRW100B.DAT
TIME/DATE OF STUDY: 10:47 07/14/2009

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

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--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 100.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 18.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.85
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) III ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF-WIDTH (FT)	CROWN TO CROSSFALL (FT)	STREET-CROSSFALL: IN- / OUT- / SIDE / SIDE / WAY	CURB HEIGHT (FT)	GUTTER WIDTH (FT)	GEOMETRIES: LIP (FT)	MANNING HIKE (FT)	FACTOR (n)
1	30.0	20.0	0.018/0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:
1. Relative Flow-Depth = 0.00 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)
SIZE PIPE WITH A FLOW CAPACITY GREATER THAN OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.
*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 50.00 TO NODE 51.00 IS CODE = 21 ✓

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 300.00
ELEVATION DATA: UPSTREAM(FEET) = 660.00 DOWNSTREAM(FEET) = 654.00

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 6.509
* 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.319
SUBAREA Tc AND LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
COMMERCIAL	B	3.03	0.30	0.100	76	6.51

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
SUBAREA RUNOFF(CFS) = 14.42
TOTAL AREA(ACRES) = 3.03 PEAK FLOW RATE(CFS) = 14.42

FLOW PROCESS FROM NODE 51.00 TO NODE 52.00 IS CODE = 81 ✓

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

MAINLINE Tc(MIN.) = 6.51
 * 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.319
 SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
COMMERCIAL	C	6.18 ✓	0.25	0.100	86

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.25
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 0.100
 SUBAREA AREA(ACRES) = 6.18 SUBAREA RUNOFF(CFS) = 29.45
 EFFECTIVE AREA(ACRES) = 9.21 AREA-AVERAGED Fm(INCH/HR) = 0.03
 AREA-AVERAGED Fp(INCH/HR) = 0.27 AREA-AVERAGED Ap = 0.10
 TOTAL AREA(ACRES) = 9.2 PEAK FLOW RATE(CFS) = 43.87

FLOW PROCESS FROM NODE 52.00 TO NODE 53.00 IS CODE = 31 ✓

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<
>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<

ELEVATION DATA: UPSTREAM(FEET) = 636.80 DOWNSTREAM(FEET) = 573.00
 FLOW LENGTH(FEET) = 200.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.2 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 34.40
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 43.87 ✓
 PIPE TRAVEL TIME(MIN.) = 0.10 Tc(MIN.) = 6.61
 LONGEST FLOWPATH FROM NODE 50.00 TO NODE 53.00 = 500.00 FEET.

FLOW PROCESS FROM NODE 53.00 TO NODE 53.00 IS CODE = 81 ✓ AREA C2

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<

MAINLINE Tc(MIN.) = 6.61
 * 100 YEAR RAINFALL INTENSITY(INCH/HR) = 5.275
 SUBAREA LOSS RATE DATA(AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL GOOD COVER "GRASS"	C	3.19 ✓	0.25	1.000	90

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.25
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
 SUBAREA AREA(ACRES) = 3.19 SUBAREA RUNOFF(CFS) = 14.43
 EFFECTIVE AREA(ACRES) = 12.40 AREA-AVERAGED Fm(INCH/HR) = 0.08
 AREA-AVERAGED Fp(INCH/HR) = 0.25 AREA-AVERAGED Ap = 0.33
 TOTAL AREA(ACRES) = 12.4 PEAK FLOW RATE(CFS) = 57.93

FLOW PROCESS FROM NODE 54.00 TO NODE 55.00 IS CODE = 21 ✓ AREA C1

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 1052.00
ELEVATION DATA: UPSTREAM (FEET) = 638.80 DOWNSTREAM (FEET) = 560.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 25.393

• 100 YEAR RAINFALL INTENSITY (INCH/HR) = 2.438

SUBAREA T_c AND LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
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NATURAL GOOD COVER "OPEN BRUSH"	A	2.95 ✓	0.40	1.000	61	25.39
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SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.40

SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 1.000

SUBAREA RUNOFF (CFS) = 5.41

TOTAL AREA (ACRES) = 2.95 PEAK FLOW RATE (CFS) = 5.41

FLOW PROCESS FROM NODE 45.00 TO NODE 46.00 IS CODE = 21 ✓ AREA C4

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 223.00
ELEVATION DATA: UPSTREAM (FEET) = 628.80 DOWNSTREAM (FEET) = 608.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$
SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 13.067

* 100 YEAR RAINFALL INTENSITY (INCH/HR) = 3.568

SUBAREA T_c AND LOSS RATE DATA (AMC III):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN	T_c (MIN.)
-------------------------------	-------------------	-----------------	--------------------	--------------------	-----------	-----------------

NATURAL GOOD COVER "GRASS"	B	3.83 ✓	0.30	1.000	80	13.07
-------------------------------	---	--------	------	-------	----	-------

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.30

SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 1.000

SUBAREA RUNOFF (CFS) = 11.27

TOTAL AREA (ACRES) = 3.83 PEAK FLOW RATE (CFS) = 11.27

=====

END OF STUDY SUMMARY:

TOTAL AREA (ACRES) = 3.8 TC (MIN.) = 13.07

EFFECTIVE AREA (ACRES) = 3.83 AREA-AVERAGED F_m (INCH/HR) = 0.30

AREA-AVERAGED F_p (INCH/HR) = 0.30 AREA-AVERAGED A_p = 1.000

PEAK FLOW RATE (CFS) = 11.27

=====

END OF RATIONAL METHOD ANALYSIS

LOSS RATE AREA A

 NON-HOMOGENEOUS WATERSHED AREA-AVERAGED LOSS RATE (Fm)
 AND LOW LOSS FRACTION ESTIMATIONS
 =====

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 Ver. 14.0 Release Date: 06/01/2007 License ID 1355

Analysis prepared by:

Fusco Engineering, Inc
 16795 Von Karman Ave. Suite 100
 Irvine, California 92606
 PH: 949-474-1960 FAX: 949-474-5315

Problem Descriptions:
 TENTATIVE TRACT 17331
 SERRANO SUMMIT
 PROPOSED CONDITION AREA - A

 *** NON-HOMOGENEOUS WATERSHED AREA-AVERAGED LOSS RATE (Fm)
 AND LOW LOSS FRACTION ESTIMATIONS FOR AMC III:
 =====

TOTAL 24-HOUR DURATION RAINFALL DEPTH = 5.63 (inches)

SOIL-COVER TYPE	AREA (Acres)	PERCENT OF PERVIOUS AREA	SCS CURVE NUMBER	LOSS RATE Fp(in./hr.)	YIELD
1	67.20	20.00	69	0.025	0.910

TOTAL AREA (Acres) = 67.20

AREA-AVERAGED LOSS RATE, \bar{F}_m (in./hr.) = 0.005

AREA-AVERAGED LOW LOSS FRACTION, \bar{Y} = 0.090
 =====

UNIT HYDROGRAPH AREA A

 SMALL AREA UNIT HYDROGRAPH MODEL

=====
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 Ver. 14.0 Release Date: 06/01/2007 License ID 1355

Analysis prepared by:

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 Problem Descriptions:
 TENTATIVE TRACT 17331
 SERRANO SUMMIT
 PROPOSED CONDITION AREA - A

RATIONAL METHOD CALIBRATION COEFFICIENT = 0.75
 TOTAL CATCHMENT AREA (ACRES) = 67.20
 SOIL-LOSS RATE, Fm, (INCH/HR) = 0.005
 LOW LOSS FRACTION = 0.090
 TIME OF CONCENTRATION (MIN.) = 7.89
 SMALL AREA PEAK Q COMPUTED USING PEAK FLOW RATE FORMULA
 ORANGE COUNTY "VALLEY" RAINFALL VALUES ARE USED
 RETURN FREQUENCY (YEARS) = 100
 5-MINUTE POINT RAINFALL VALUE (INCHES) = 0.52
 30-MINUTE POINT RAINFALL VALUE (INCHES) = 1.09
 1-HOUR POINT RAINFALL VALUE (INCHES) = 1.45
 3-HOUR POINT RAINFALL VALUE (INCHES) = 2.43
 6-HOUR POINT RAINFALL VALUE (INCHES) = 3.36
 24-HOUR POINT RAINFALL VALUE (INCHES) = 5.63

 TOTAL CATCHMENT RUNOFF VOLUME (ACRE-FEET) = 22.97
 TOTAL CATCHMENT SOIL-LOSS VOLUME (ACRE-FEET) = 8.56

TIME (HOURS)	VOLUME (AF)	Q (CFS)	0.	62.5	125.0	187.5	250.0
0.09	0.0152	4.15	Q
0.22	0.0604	4.17	Q
0.35	0.1058	4.20	Q
0.48	0.1515	4.21	Q
0.61	0.1975	4.24	Q
0.75	0.2437	4.26	Q

0.88	0.2902	4.29	Q
1.01	0.3369	4.31	Q
1.14	0.3839	4.34	Q
1.27	0.4312	4.36	Q
1.40	0.4787	4.39	Q
1.54	0.5266	4.41	Q
1.67	0.5747	4.45	Q
1.80	0.6231	4.46	Q
1.93	0.6719	4.50	Q
2.06	0.7209	4.52	Q
2.19	0.7702	4.56	Q
2.32	0.8198	4.58	Q
2.46	0.8698	4.62	Q
2.59	0.9201	4.64	Q
2.72	0.9707	4.68	Q
2.85	1.0216	4.70	Q
2.98	1.0728	4.74	Q
3.11	1.1244	4.76	Q
3.24	1.1764	4.80	Q
3.38	1.2287	4.82	Q
3.51	1.2813	4.87	Q
3.64	1.3344	4.89	Q
3.77	1.3878	4.94	Q
3.90	1.4415	4.96	Q
4.03	1.4957	5.01	Q
4.16	1.5502	5.03	Q
4.30	1.6052	5.08	Q
4.43	1.6605	5.11	Q
4.56	1.7163	5.16	Q
4.69	1.7724	5.18	Q
4.82	1.8290	5.23	Q
4.95	1.8861	5.26	Q
5.09	1.9435	5.32	Q
5.22	2.0015	5.34	Q
5.35	2.0599	5.40	Q
5.48	2.1187	5.43	Q
5.61	2.1781	5.49	Q
5.74	2.2379	5.52	Q
5.87	2.2983	5.58	Q
6.01	2.3591	5.61	Q
6.14	2.4205	5.68	Q
6.27	2.4824	5.71	Q
6.40	2.5448	5.78	Q
6.53	2.6078	5.81	Q
6.66	2.6714	5.89	Q
6.80	2.7355	5.92	Q
6.93	2.8003	6.00	Q
7.06	2.8657	6.03	Q
7.19	2.9316	6.11	Q
7.32	2.9983	6.15	Q
7.45	3.0655	6.23	Q
7.58	3.1335	6.27	.Q
7.72	3.2021	6.36	.Q
7.85	3.2715	6.40	.Q
7.98	3.3415	6.49	.Q
8.11	3.4123	6.54	.Q
8.24	3.4839	6.63	.Q

8.37	3.5562	6.68	.Q
8.50	3.6294	6.78	.Q
8.64	3.7034	6.83	.Q
8.77	3.7782	6.94	.Q
8.90	3.8539	6.99	.Q
9.03	3.9306	7.11	.Q
9.16	4.0081	7.16	.Q
9.29	4.0866	7.28	.Q
9.43	4.1661	7.35	.Q
9.56	4.2466	7.47	.Q
9.69	4.3282	7.54	.Q
9.82	4.4109	7.68	.Q
9.95	4.4947	7.75	.Q
10.08	4.5797	7.89	.Q
10.21	4.6658	7.97	.Q
10.35	4.7533	8.12	.Q
10.48	4.8420	8.20	.Q
10.61	4.9321	8.37	.Q
10.74	5.0235	8.46	.Q
10.87	5.1165	8.64	.Q
11.00	5.2109	8.74	.Q
11.13	5.3070	8.94	.Q
11.27	5.4047	9.04	.Q
11.40	5.5041	9.26	.Q
11.53	5.6054	9.37	.Q
11.66	5.7085	9.61	.Q
11.79	5.8136	9.73	.Q
11.92	5.9208	10.00	.Q
12.05	6.0302	10.13	.Q
12.19	6.1565	13.12	. Q
12.32	6.3000	13.28	. Q
12.45	6.4462	13.63	. Q
12.58	6.5953	13.81	. Q
12.71	6.7474	14.19	. Q
12.84	6.9028	14.40	. Q
12.98	7.0616	14.83	. Q
13.11	7.2240	15.06	. Q
13.24	7.3904	15.56	. Q
13.37	7.5609	15.82	. Q
13.50	7.7359	16.39	. Q
13.63	7.9158	16.70	. Q
13.76	8.1009	17.37	. Q
13.90	8.2917	17.74	. Q
14.03	8.4888	18.54	. Q
14.16	8.6931	19.06	. Q
14.29	8.9056	20.05	. Q
14.42	9.1265	20.60	. Q
14.55	9.3571	21.83	. Q
14.68	9.5982	22.53	. Q
14.82	9.8518	24.15	. Q
14.95	10.1194	25.09	. Q
15.08	10.4043	27.34	. Q
15.21	10.7088	28.70	. Q
15.34	11.0394	32.14	. Q
15.47	11.3868	31.78	. Q
15.61	11.7562	36.20	. Q
15.74	12.1746	40.80	. Q

15.87	12.7123	58.16	.	Q.	.	.	.
16.00	13.4605	79.52	.	.	Q	.	.
16.13	15.1987	240.37	Q
16.26	16.7631	47.52	.	Q	.	.	.
16.39	17.1994	32.78	.	Q	.	.	.
16.53	17.5421	30.28	.	Q	.	.	.
16.66	17.8487	26.15	.	Q	.	.	.
16.79	18.1174	23.30	.	Q	.	.	.
16.92	18.3591	21.19	.	Q	.	.	.
17.05	18.5805	19.55	.	Q	.	.	.
17.18	18.7852	18.12	.	Q	.	.	.
17.32	18.9762	17.03	.	Q	.	.	.
17.45	19.1562	16.10	.	Q	.	.	.
17.58	19.3269	15.30	.	Q	.	.	.
17.71	19.4894	14.61	.	Q	.	.	.
17.84	19.6448	14.00	.	Q	.	.	.
17.97	19.7940	13.45	.	Q	.	.	.
18.10	19.9321	11.96	.	Q	.	.	.
18.24	20.0507	9.86	.	Q	.	.	.
18.37	20.1558	9.49	.	Q	.	.	.
18.50	20.2571	9.15	.	Q	.	.	.
18.63	20.3548	8.84	.	Q	.	.	.
18.76	20.4493	8.55	.	Q	.	.	.
18.89	20.5408	8.29	.	Q	.	.	.
19.02	20.6295	8.04	.	Q	.	.	.
19.16	20.7157	7.82	.	Q	.	.	.
19.29	20.7995	7.61	.	Q	.	.	.
19.42	20.8811	7.41	.	Q	.	.	.
19.55	20.9606	7.22	.	Q	.	.	.
19.68	21.0382	7.05	.	Q	.	.	.
19.81	21.1139	6.89	.	Q	.	.	.
19.94	21.1879	6.73	.	Q	.	.	.
20.08	21.2603	6.59	.	Q	.	.	.
20.21	21.3311	6.45	.	Q	.	.	.
20.34	21.4004	6.32	.	Q	.	.	.
20.47	21.4684	6.19	.	Q	.	.	.
20.60	21.5350	6.07	.	Q	.	.	.
20.73	21.6004	5.96	.	Q	.	.	.
20.87	21.6645	5.85	.	Q	.	.	.
21.00	21.7276	5.75	.	Q	.	.	.
21.13	21.7895	5.65	.	Q	.	.	.
21.26	21.8503	5.55	.	Q	.	.	.
21.39	21.9101	5.46	.	Q	.	.	.
21.52	21.9690	5.37	.	Q	.	.	.
21.65	22.0270	5.29	.	Q	.	.	.
21.79	22.0840	5.21	.	Q	.	.	.
21.92	22.1402	5.13	.	Q	.	.	.
22.05	22.1955	5.05	.	Q	.	.	.
22.18	22.2501	4.98	.	Q	.	.	.
22.31	22.3038	4.91	.	Q	.	.	.
22.44	22.3568	4.84	.	Q	.	.	.
22.58	22.4091	4.78	.	Q	.	.	.
22.71	22.4607	4.72	.	Q	.	.	.
22.84	22.5117	4.66	.	Q	.	.	.
22.97	22.5619	4.60	.	Q	.	.	.
23.10	22.6116	4.54	.	Q	.	.	.
23.23	22.6606	4.48	.	Q	.	.	.

23.36	22.7090	4.43	Q
23.50	22.7569	4.38	Q
23.63	22.8042	4.33	Q
23.76	22.8509	4.28	Q
23.89	22.8971	4.23	Q
24.02	22.9428	4.18	Q
24.15	22.9655	0.00	Q

Serrano Area A

Prepared by FUSCOE Engineering
 HydroCAD® 9.10 s/n 05904 © 2009 HydroCAD Software Solutions LLC

Type II 24-hr Rainfall=5.63", AMC=3
 Printed 2/23/2010

Summary for Pond 2P: Area A Detention Basin

Inflow Area = 67.200 ac, 0.00% Impervious, Inflow Depth = 4.17"
 Inflow = 204.19 cfs @ 16.10 hrs, Volume= 23.363 af
 Outflow = 133.55 cfs @ 16.19 hrs, Volume= 23.410 af, Atten= 35%, Lag= 5.3 min
 Primary = 133.55 cfs @ 16.19 hrs, Volume= 23.410 af

Routing by Stor-Ind method, Time Span= 0.00-26.00 hrs, dt= 0.13 hrs
 Peak Elev= 590.60' @ 16.19 hrs Surf.Area= 1.248 ac Storage= 0.735 af

Plug-Flow detention time= (not calculated: outflow precedes inflow)
 Center-of-Mass det. time= 1.1 min (835.4 - 834.3)

Volume	Invert	Avail.Storage	Storage Description
#1	590.00'	7.000 af	Custom Stage Data (Prismatic) Listed below (Recalc)

Elevation (feet)	Surf.Area (acres)	Inc.Store (acre-feet)	Cum.Store (acre-feet)
590.00	1.200	0.000	0.000
591.00	1.280	1.240	1.240
592.00	1.360	1.320	2.560
593.00	1.440	1.400	3.960
594.00	1.520	1.480	5.440
595.00	1.600	1.560	7.000

Device	Routing	Invert	Outlet Devices
#1	Primary	583.00'	42.0" Round Culvert L= 400.0' RCP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 583.00' / 512.00' S= 0.1775 ' / n= 0.013
#2	Primary	590.00'	48.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads

Primary OutFlow Max=127.45 cfs @ 16.19 hrs HW=590.53' (Free Discharge)
 1=Culvert (Inlet Controls 111.41 cfs @ 11.58 fps)
 2=Orifice/Grate (Weir Controls 16.04 cfs @ 2.39 fps)

LOSS RATE CIVIC CENTER

 NON-HOMOGENEOUS WATERSHED AREA-AVERAGED LOSS RATE (Fm)
 AND LOW LOSS FRACTION ESTIMATIONS
 =====

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Problem Descriptions:
 TENTATIVE TRACT 17331
 SERRANO SUMMIT
 PROPOSED CONDITION CIVIC CENTER

 *** NON-HOMOGENEOUS WATERSHED AREA-AVERAGED LOSS RATE (Fm)
 AND LOW LOSS FRACTION ESTIMATIONS FOR AMC III:
 =====

TOTAL 24-HOUR DURATION RAINFALL DEPTH = 5.63 (inches)

SOIL-COVER TYPE	AREA (Acres)	PERCENT OF PERVIOUS AREA	SCS CURVE NUMBER	LOSS RATE Fp(in./hr.)	YIELD
1	12.40	12.00	69	0.250	0.929

TOTAL AREA (Acres) = 12.40

AREA-AVERAGED LOSS RATE, \bar{F}_m (in./hr.) = 0.030

AREA-AVERAGED LOW LOSS FRACTION, \bar{Y} = 0.071

=====

UNIT HYDROGRAPH CIVIC CENTER

SMALL AREA UNIT HYDROGRAPH MODEL

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Ver. 14.0 Release Date: 06/01/2007 License ID 1355

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Problem Descriptions:

TENTATIVE TRACT 17331
SERRANO SUMMIT
PROPOSED CONDITION CIVIC CENTER

RATIONAL METHOD CALIBRATION COEFFICIENT = 0.90
TOTAL CATCHMENT AREA (ACRES) = 12.40
SOIL-LOSS RATE, Fm, (INCH/HR) = 0.030
LOW LOSS FRACTION = 0.071
TIME OF CONCENTRATION (MIN.) = 6.61
SMALL AREA PEAK Q COMPUTED USING PEAK FLOW RATE FORMULA
ORANGE COUNTY "VALLEY" RAINFALL VALUES ARE USED
RETURN FREQUENCY (YEARS) = 100
5-MINUTE POINT RAINFALL VALUE (INCHES) = 0.52
30-MINUTE POINT RAINFALL VALUE (INCHES) = 1.09
1-HOUR POINT RAINFALL VALUE (INCHES) = 1.45
3-HOUR POINT RAINFALL VALUE (INCHES) = 2.43
6-HOUR POINT RAINFALL VALUE (INCHES) = 3.36
24-HOUR POINT RAINFALL VALUE (INCHES) = 5.63

TOTAL CATCHMENT RUNOFF VOLUME (ACRE-FEET) = 4.90
TOTAL CATCHMENT SOIL-LOSS VOLUME (ACRE-FEET) = 0.92

TIME (HOURS)	VOLUME (AF)	Q (CFS)	0.	15.0	30.0	45.0	60.0
0.03	0.0000	0.00	Q
0.14	0.0041	0.91	Q
0.25	0.0124	0.91	Q
0.36	0.0207	0.91	Q
0.47	0.0291	0.92	Q
0.58	0.0375	0.92	Q

0.69	0.0459	0.93	Q
0.80	0.0543	0.93	Q
0.91	0.0628	0.94	Q
1.02	0.0714	0.94	Q
1.13	0.0800	0.95	Q
1.24	0.0886	0.95	Q
1.35	0.0972	0.95	Q
1.46	0.1059	0.96	Q
1.57	0.1147	0.96	Q
1.68	0.1235	0.97	Q
1.79	0.1323	0.97	Q
1.90	0.1412	0.98	Q
2.01	0.1501	0.98	Q
2.12	0.1590	0.99	Q
2.23	0.1680	0.99	Q
2.34	0.1771	1.00	Q
2.45	0.1861	1.00	Q
2.56	0.1953	1.01	Q
2.67	0.2045	1.01	Q
2.78	0.2137	1.02	Q
2.89	0.2230	1.02	Q
3.00	0.2323	1.03	Q
3.11	0.2417	1.03	Q
3.22	0.2511	1.04	Q
3.33	0.2606	1.04	Q
3.44	0.2701	1.05	Q
3.55	0.2797	1.06	Q
3.66	0.2893	1.06	Q
3.77	0.2990	1.07	Q
3.88	0.3088	1.07	Q
3.99	0.3186	1.08	Q
4.10	0.3284	1.08	Q
4.21	0.3383	1.09	Q
4.32	0.3483	1.10	Q
4.43	0.3583	1.11	Q
4.54	0.3684	1.11	Q
4.65	0.3785	1.12	Q
4.76	0.3888	1.12	Q
4.87	0.3990	1.13	Q
4.98	0.4094	1.14	Q
5.09	0.4198	1.15	Q
5.20	0.4302	1.15	Q
5.31	0.4408	1.16	Q
5.42	0.4514	1.17	Q
5.53	0.4620	1.18	Q
5.64	0.4728	1.18	Q
5.75	0.4836	1.19	Q
5.86	0.4945	1.20	Q
5.97	0.5054	1.21	Q
6.08	0.5164	1.21	Q
6.20	0.5275	1.23	Q
6.31	0.5387	1.23	Q
6.42	0.5500	1.24	Q
6.53	0.5613	1.25	Q
6.64	0.5728	1.26	Q
6.75	0.5843	1.27	Q
6.86	0.5959	1.28	Q

6.97	0.6076	1.29	Q
7.08	0.6193	1.30	Q
7.19	0.6312	1.31	Q
7.30	0.6432	1.32	Q
7.41	0.6552	1.33	Q
7.52	0.6674	1.34	Q
7.63	0.6796	1.35	Q
7.74	0.6919	1.36	Q
7.85	0.7044	1.37	Q
7.96	0.7170	1.39	Q
8.07	0.7296	1.39	Q
8.18	0.7424	1.41	Q
8.29	0.7553	1.42	Q
8.40	0.7683	1.44	Q
8.51	0.7814	1.44	Q
8.62	0.7946	1.46	Q
8.73	0.8080	1.47	Q
8.84	0.8215	1.49	Q
8.95	0.8351	1.50	Q
9.06	0.8488	1.52	.Q
9.17	0.8627	1.53	.Q
9.28	0.8767	1.55	.Q
9.39	0.8909	1.56	.Q
9.50	0.9052	1.58	.Q
9.61	0.9196	1.59	.Q
9.72	0.9343	1.62	.Q
9.83	0.9490	1.63	.Q
9.94	0.9640	1.65	.Q
10.05	0.9791	1.67	.Q
10.16	0.9944	1.69	.Q
10.27	1.0098	1.70	.Q
10.38	1.0255	1.73	.Q
10.49	1.0413	1.75	.Q
10.60	1.0574	1.78	.Q
10.71	1.0736	1.79	.Q
10.82	1.0900	1.82	.Q
10.93	1.1067	1.84	.Q
11.04	1.1236	1.87	.Q
11.15	1.1407	1.89	.Q
11.26	1.1581	1.93	.Q
11.37	1.1757	1.94	.Q
11.48	1.1936	1.98	.Q
11.59	1.2117	2.00	.Q
11.70	1.2302	2.05	.Q
11.81	1.2489	2.07	.Q
11.92	1.2679	2.11	.Q
12.03	1.2872	2.14	.Q
12.14	1.3094	2.74	.Q
12.25	1.3345	2.77	.Q
12.36	1.3600	2.83	.Q
12.47	1.3858	2.86	.Q
12.58	1.4121	2.92	.Q
12.70	1.4389	2.95	.Q
12.81	1.4661	3.02	. Q
12.92	1.4938	3.06	. Q
13.03	1.5220	3.14	. Q
13.14	1.5507	3.18	. Q

13.25	1.5800	3.26	. Q
13.36	1.6100	3.31	. Q
13.47	1.6406	3.41	. Q
13.58	1.6718	3.46	. Q
13.69	1.7039	3.57	. Q
13.80	1.7367	3.63	. Q
13.91	1.7703	3.76	. Q
14.02	1.8049	3.83	. Q
14.13	1.8406	4.00	. Q
14.24	1.8774	4.09	. Q
14.35	1.9155	4.27	. Q
14.46	1.9548	4.37	. Q
14.57	1.9956	4.60	. Q
14.68	2.0381	4.74	. Q
14.79	2.0826	5.04	. Q
14.90	2.1293	5.21	. Q
15.01	2.1784	5.60	. Q
15.12	2.2305	5.83	. Q
15.23	2.2860	6.38	. Q
15.34	2.3456	6.71	. Q
15.45	2.4061	6.59	. Q
15.56	2.4686	7.12	. Q
15.67	2.5403	8.62	. Q
15.78	2.6240	9.77	. Q
15.89	2.7323	14.02	.	. Q	.	.	.
16.00	2.8838	19.26	.	. Q	.	.	.
16.11	3.2391	58.78 Q
16.22	3.5586	11.41	.	. Q	.	.	.
16.33	3.6459	7.78	. Q
16.44	3.7133	7.02	. Q
16.55	3.7730	6.09	. Q
16.66	3.8252	5.39	. Q
16.77	3.8720	4.88	. Q
16.88	3.9146	4.48	. Q
16.99	3.9540	4.17	. Q
17.10	3.9908	3.91	. Q
17.21	4.0254	3.70	. Q
17.32	4.0583	3.52	. Q
17.43	4.0896	3.36	. Q
17.54	4.1195	3.22	. Q
17.65	4.1483	3.10	. Q
17.76	4.1760	2.99	. Q
17.87	4.2027	2.89	. Q
17.98	4.2286	2.80	. Q
18.09	4.2523	2.42	. Q
18.20	4.2728	2.09	. Q
18.31	4.2916	2.02	. Q
18.42	4.3097	1.96	. Q
18.53	4.3273	1.91	. Q
18.64	4.3445	1.86	. Q
18.75	4.3611	1.81	. Q
18.86	4.3774	1.76	. Q
18.97	4.3932	1.72	. Q
19.08	4.4087	1.68	. Q
19.19	4.4238	1.64	. Q
19.31	4.4386	1.61	. Q
19.42	4.4530	1.57	. Q

19.53	4.4672	1.54	.Q
19.64	4.4811	1.51	.Q
19.75	4.4947	1.48	Q
19.86	4.5080	1.45	Q
19.97	4.5212	1.43	Q
20.08	4.5340	1.40	Q
20.19	4.5467	1.38	Q
20.30	4.5592	1.36	Q
20.41	4.5714	1.33	Q
20.52	4.5835	1.31	Q
20.63	4.5953	1.29	Q
20.74	4.6070	1.27	Q
20.85	4.6185	1.26	Q
20.96	4.6299	1.24	Q
21.07	4.6411	1.22	Q
21.18	4.6521	1.20	Q
21.29	4.6630	1.19	Q
21.40	4.6737	1.17	Q
21.51	4.6843	1.16	Q
21.62	4.6948	1.14	Q
21.73	4.7051	1.13	Q
21.84	4.7153	1.11	Q
21.95	4.7254	1.10	Q
22.06	4.7354	1.09	Q
22.17	4.7452	1.08	Q
22.28	4.7550	1.06	Q
22.39	4.7646	1.05	Q
22.50	4.7741	1.04	Q
22.61	4.7836	1.03	Q
22.72	4.7929	1.02	Q
22.83	4.8021	1.01	Q
22.94	4.8112	1.00	Q
23.05	4.8203	0.99	Q
23.16	4.8292	0.98	Q
23.27	4.8381	0.97	Q
23.38	4.8469	0.96	Q
23.49	4.8556	0.95	Q
23.60	4.8642	0.94	Q
23.71	4.8728	0.93	Q
23.82	4.8812	0.93	Q
23.93	4.8896	0.92	Q
24.04	4.8979	0.91	Q
24.15	4.9021	0.00	Q

Serrano Civic Center

Prepared by FUSCOE Engineering

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Type II 24-hr Rainfall=5.63", AMC=3

Printed 2/23/2010

Summary for Pond 2P: Civic Center Detention Basin

Inflow Area = 12.400 ac, 0.00% Impervious, Inflow Depth = 4.79"
 Inflow = 52.55 cfs @ 16.16 hrs, Volume= 4.954 af
 Outflow = 33.15 cfs @ 16.23 hrs, Volume= 4.945 af, Atten= 37%, Lag= 4.0 min
 Primary = 33.15 cfs @ 16.23 hrs, Volume= 4.945 af

Routing by Stor-Ind method, Time Span= 0.00-25.00 hrs, dt= 0.05 hrs
 Peak Elev= 576.21' @ 16.23 hrs Surf.Area= 0.158 ac Storage= 0.381 af

Plug-Flow detention time= 14.8 min calculated for 4.945 af (100% of inflow)
 Center-of-Mass det. time= 13.7 min (849.6 - 835.9)

Volume	Invert	Avail.Storage	Storage Description
#1	573.00'	0.513 af	30.00'W x 120.00'L x 4.00'H Prismatic Z=3.0

Device	Routing	Invert	Outlet Devices
#1	Primary	573.00'	30.0" Round Culvert L= 50.0' RCP, square edge headwall, Ke= 0.500 Inlet / Outlet Invert= 573.00' / 571.00' S= 0.0400 '/ Cc= 0.900 n= 0.013

Primary OutFlow Max=32.65 cfs @ 16.23 hrs HW=576.16' (Free Discharge)
 ←**1=Culvert** (Inlet Controls 32.65 cfs @ 6.65 fps)

**AREA A EXISTING 2 YEAR
HYDROLOGY AND HYDROGRAPH**

RATIONAL METHOD HYDROLOGY COMPUTER PROGRAM PACKAGE
(Reference: 1986 ORANGE COUNTY HYDROLOGY CRITERION)
(c) Copyright 1983-2007 Advanced Engineering Software (aes)
Ver. 13.5 Release Date: 02/06/2007 License ID 1355

Analysis prepared by:

Fusco Engineering, Inc
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Irvine, California 92606
PH: 949-474-1960 FAX: 949-474-5315

***** DESCRIPTION OF STUDY *****

* IRWD SITE - AREA A *
* 2 YEAR EXISTING HYDROLOGY *
* *

FILE NAME: IRWD02A.DAT
TIME/DATE OF STUDY: 10:18 03/09/2010

=====

USER SPECIFIED HYDROLOGY AND HYDRAULIC MODEL INFORMATION:

=====

--*TIME-OF-CONCENTRATION MODEL*--

USER SPECIFIED STORM EVENT(YEAR) = 2.00
SPECIFIED MINIMUM PIPE SIZE(INCH) = 8.00
SPECIFIED PERCENT OF GRADIENTS(DECIMAL) TO USE FOR FRICTION SLOPE = 0.85
DATA BANK RAINFALL USED
ANTECEDENT MOISTURE CONDITION (AMC) II ASSUMED FOR RATIONAL METHOD

USER-DEFINED STREET-SECTIONS FOR COUPLED PIPEFLOW AND STREETFLOW MODEL

NO.	HALF-	CROWN TO	STREET-CROSSFALL:			CURB	GUTTER-GEOMETRIES:		MANNING	
	WIDTH	CROSSFALL	IN-	/	OUT-/PARK-	HEIGHT	WIDTH	LIP	HIKE	FACTOR
	(FT)	(FT)	SIDE	/	SIDE/ WAY	(FT)	(FT)	(FT)	(FT)	(n)
1	30.0	20.0	0.018	/	0.018/0.020	0.67	2.00	0.0313	0.167	0.0150

GLOBAL STREET FLOW-DEPTH CONSTRAINTS:

1. Relative Flow-Depth = 0.33 FEET
as (Maximum Allowable Street Flow Depth) - (Top-of-Curb)
2. (Depth)*(Velocity) Constraint = 6.0 (FT*FT/S)

*SIZE PIPE WITH A FLOW CAPACITY GREATER THAN
OR EQUAL TO THE UPSTREAM TRIBUTARY PIPE.*

*USER-SPECIFIED MINIMUM TOPOGRAPHIC SLOPE ADJUSTMENT NOT SELECTED

FLOW PROCESS FROM NODE 10.00 TO NODE 11.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

INITIAL SUBAREA FLOW-LENGTH(FEET) = 252.00
ELEVATION DATA: UPSTREAM(FEET) = 706.50 DOWNSTREAM(FEET) = 688.30

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20

SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 8.109

* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.715

SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
NATURAL POOR COVER "GRASS"	C	0.55	0.25	1.000	86	8.11
NATURAL POOR COVER "GRASS"	B	0.22	0.30	1.000	78	8.11

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.26
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
SUBAREA RUNOFF(CFS) = 1.01
TOTAL AREA(ACRES) = 0.77 PEAK FLOW RATE(CFS) = 1.01

FLOW PROCESS FROM NODE 11.00 TO NODE 12.00 IS CODE = 91

>>>>>COMPUTE "V" GUTTER FLOW TRAVEL TIME THRU SUBAREA<<<<<

=====

UPSTREAM NODE ELEVATION(FEET) = 688.30
DOWNSTREAM NODE ELEVATION(FEET) = 658.40
CHANNEL LENGTH THRU SUBAREA(FEET) = 1247.00
"V" GUTTER WIDTH(FEET) = 5.00 GUTTER HIKE(FEET) = 0.050
PAVEMENT LIP(FEET) = 0.010 MANNING'S N = .0500
PAVEMENT CROSSFALL(DECIMAL NOTATION) = 0.07000
MAXIMUM DEPTH(FEET) = 3.00
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.081
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL POOR COVER "GRASS"	B	9.28	0.30	1.000	78
NATURAL POOR COVER "GRASS"	C	18.28	0.25	1.000	86

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.27
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 9.05
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.07
AVERAGE FLOW DEPTH(FEET) = 0.45 FLOOD WIDTH(FEET) = 16.26
"V" GUTTER FLOW TRAVEL TIME(MIN.) = 10.02 Tc(MIN.) = 18.13
SUBAREA AREA(ACRES) = 27.56 SUBAREA RUNOFF(CFS) = 20.19
EFFECTIVE AREA(ACRES) = 28.33 AREA-AVERAGED Fm(INCH/HR) = 0.27
AREA-AVERAGED Fp(INCH/HR) = 0.27 AREA-AVERAGED Ap = 1.00
TOTAL AREA(ACRES) = 28.3 PEAK FLOW RATE(CFS) = 20.75

END OF SUBAREA "V" GUTTER HYDRAULICS:

DEPTH(FEET) = 0.65 FLOOD WIDTH(FEET) = 21.92
FLOW VELOCITY(FEET/SEC.) = 2.55 DEPTH*VELOCITY(FT*FT/SEC) = 1.66
LONGEST FLOWPATH FROM NODE 10.00 TO NODE 12.00 = 1499.00 FEET.

FLOW PROCESS FROM NODE 12.00 TO NODE 13.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<

>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

ELEVATION DATA: UPSTREAM(FEET) = 643.00 DOWNSTREAM(FEET) = 636.00
 FLOW LENGTH(FEET) = 106.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 12.6 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 15.76
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 20.75
 PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 18.24
 LONGEST FLOWPATH FROM NODE 10.00 TO NODE 13.00 = 1605.00 FEET.

 FLOW PROCESS FROM NODE 30.00 TO NODE 13.00 IS CODE = 81

>>>>ADDITION OF SUBAREA TO MAINLINE PEAK FLOW<<<<<

=====

MAINLINE Tc(MIN.) = 18.24
 * 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.077
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL POOR COVER "CHAPARRAL,NARROWLEAF"	B	0.63	0.30	1.000	82
NATURAL POOR COVER "CHAPARRAL,NARROWLEAF"	C	3.06	0.25	1.000	88

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.26
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
 SUBAREA AREA(ACRES) = 3.69 SUBAREA RUNOFF(CFS) = 2.72
 EFFECTIVE AREA(ACRES) = 32.02 AREA-AVERAGED Fm(INCH/HR) = 0.27
 AREA-AVERAGED Fp(INCH/HR) = 0.27 AREA-AVERAGED Ap = 1.00
 TOTAL AREA(ACRES) = 32.0 PEAK FLOW RATE(CFS) = 23.37

 FLOW PROCESS FROM NODE 13.00 TO NODE 13.50 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 636.00 DOWNSTREAM(FEET) = 615.00
 FLOW LENGTH(FEET) = 143.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 18.0 INCH PIPE IS 10.4 INCHES
 PIPE-FLOW VELOCITY (FEET/SEC.) = 22.20
 ESTIMATED PIPE DIAMETER(INCH) = 18.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 23.37
 PIPE TRAVEL TIME(MIN.) = 0.11 Tc(MIN.) = 18.35
 LONGEST FLOWPATH FROM NODE 10.00 TO NODE 13.50 = 1748.00 FEET.

 FLOW PROCESS FROM NODE 13.50 TO NODE 14.00 IS CODE = 91

>>>>COMPUTE "V" GUTTER FLOW TRAVEL TIME THRU SUBAREA<<<<<

=====

UPSTREAM NODE ELEVATION(FEET) = 615.00
 DOWNSTREAM NODE ELEVATION(FEET) = 596.00
 CHANNEL LENGTH THRU SUBAREA(FEET) = 194.00
 "V" GUTTER WIDTH(FEET) = 5.00 GUTTER HIKE(FEET) = 0.050
 PAVEMENT LIP(FEET) = 0.010 MANNING'S N = .0150
 PAVEMENT CROSSFALL(DECIMAL NOTATION) = 0.12500
 MAXIMUM DEPTH(FEET) = 3.00

* 2 YEAR RAINFALL INTENSITY (INCH/HR) = 1.064

SUBAREA LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL FAIR COVER					
"CHAPARRAL, NARROWLEAF"	A	0.53	0.40	1.000	55
NATURAL FAIR COVER					
"CHAPARRAL, NARROWLEAF"	B	1.63	0.30	1.000	72
NATURAL FAIR COVER					
"CHAPARRAL, NARROWLEAF"	C	0.03	0.25	1.000	81

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.32
SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 1.000
TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 24.10
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 12.08
AVERAGE FLOW DEPTH (FEET) = 0.32 FLOOD WIDTH (FEET) = 9.12
"V" GUTTER FLOW TRAVEL TIME (MIN.) = 0.27 T_c (MIN.) = 18.62
SUBAREA AREA (ACRES) = 2.19 SUBAREA RUNOFF (CFS) = 1.46
EFFECTIVE AREA (ACRES) = 34.21 AREA-AVERAGED F_m (INCH/HR) = 0.27
AREA-AVERAGED F_p (INCH/HR) = 0.27 AREA-AVERAGED A_p = 1.00
TOTAL AREA (ACRES) = 34.2 PEAK FLOW RATE (CFS) = 24.47

END OF SUBAREA "V" GUTTER HYDRAULICS:

DEPTH (FEET) = 0.32 FLOOD WIDTH (FEET) = 9.17
FLOW VELOCITY (FEET/SEC.) = 12.11 DEPTH*VELOCITY (FT*FT/SEC) = 3.88
LONGEST FLOWPATH FROM NODE 10.00 TO NODE 14.00 = 1942.00 FEET.

FLOW PROCESS FROM NODE 14.00 TO NODE 14.00 IS CODE = 1

>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 1 ARE:
TIME OF CONCENTRATION (MIN.) = 18.62
RAINFALL INTENSITY (INCH/HR) = 1.06
AREA-AVERAGED F_m (INCH/HR) = 0.27
AREA-AVERAGED F_p (INCH/HR) = 0.27
AREA-AVERAGED A_p = 1.00
EFFECTIVE STREAM AREA (ACRES) = 34.21
TOTAL STREAM AREA (ACRES) = 34.21
PEAK FLOW RATE (CFS) AT CONFLUENCE = 24.47

FLOW PROCESS FROM NODE 31.00 TO NODE 32.00 IS CODE = 21

>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH (FEET) = 365.00
ELEVATION DATA: UPSTREAM (FEET) = 696.80 DOWNSTREAM (FEET) = 623.00

$T_c = K * [(LENGTH ** 3.00) / (ELEVATION CHANGE)] ** 0.20$

SUBAREA ANALYSIS USED MINIMUM T_c (MIN.) = 10.294

* 2 YEAR RAINFALL INTENSITY (INCH/HR) = 1.496

SUBAREA T_c AND LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	T_c (MIN.)
-------------------------------	-------------------	-----------------	-----------------	-----------------	-----------	-----------------

NATURAL FAIR COVER
 "CHAPARRAL, NARROWLEAF" B 0.48 0.30 1.000 72 10.29
 NATURAL FAIR COVER
 "CHAPARRAL, NARROWLEAF" C 1.87 0.25 1.000 81 10.29
 SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.26
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 1.000
 SUBAREA RUNOFF(CFS) = 2.61
 TOTAL AREA(ACRES) = 2.35 PEAK FLOW RATE(CFS) = 2.61

 FLOW PROCESS FROM NODE 32.00 TO NODE 33.00 IS CODE = 31

>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<
 >>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 618.00 DOWNSTREAM(FEET) = 601.00
 FLOW LENGTH(FEET) = 116.00 MANNING'S N = 0.013
 DEPTH OF FLOW IN 9.0 INCH PIPE IS 4.2 INCHES
 PIPE-FLOW VELOCITY(FEET/SEC.) = 12.85
 ESTIMATED PIPE DIAMETER(INCH) = 9.00 NUMBER OF PIPES = 1
 PIPE-FLOW(CFS) = 2.61
 PIPE TRAVEL TIME(MIN.) = 0.15 T_c (MIN.) = 10.44
 LONGEST FLOWPATH FROM NODE 31.00 TO NODE 33.00 = 481.00 FEET.

 FLOW PROCESS FROM NODE 33.00 TO NODE 14.00 IS CODE = 91

>>>>COMPUTE "V" GUTTER FLOW TRAVEL TIME THRU SUBAREA<<<<<

=====

UPSTREAM NODE ELEVATION(FEET) = 601.00
 DOWNSTREAM NODE ELEVATION(FEET) = 596.00
 CHANNEL LENGTH THRU SUBAREA(FEET) = 76.00
 "V" GUTTER WIDTH(FEET) = 5.00 GUTTER HIKE(FEET) = 0.050
 PAVEMENT LIP(FEET) = 0.010 MANNING'S N = .0500
 PAVEMENT CROSSFALL(DECIMAL NOTATION) = 0.12500
 MAXIMUM DEPTH(FEET) = 3.00
 * 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.440
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN
NATURAL FAIR COVER "CHAPARRAL, NARROWLEAF"	B	0.01	0.30	1.000	72

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 1.000
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 2.62
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 2.30
 AVERAGE FLOW DEPTH(FEET) = 0.21 FLOOD WIDTH(FEET) = 7.47
 "V" GUTTER FLOW TRAVEL TIME(MIN.) = 0.55 T_c (MIN.) = 10.99
 SUBAREA AREA(ACRES) = 0.01 SUBAREA RUNOFF(CFS) = 0.01
 EFFECTIVE AREA(ACRES) = 2.36 AREA-AVERAGED F_m (INCH/HR) = 0.26
 AREA-AVERAGED F_p (INCH/HR) = 0.26 AREA-AVERAGED A_p = 1.00
 TOTAL AREA(ACRES) = 2.4 PEAK FLOW RATE(CFS) = 2.61
 NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

END OF SUBAREA "V" GUTTER HYDRAULICS:

DEPTH(FEET) = 0.21 FLOOD WIDTH(FEET) = 7.45
 FLOW VELOCITY(FEET/SEC.) = 2.32 DEPTH*VELOCITY(FT*FT/SEC) = 0.49

LONGEST FLOWPATH FROM NODE 31.00 TO NODE 14.00 = 557.00 FEET.

FLOW PROCESS FROM NODE 14.00 TO NODE 14.00 IS CODE = 1

>>>>>DESIGNATE INDEPENDENT STREAM FOR CONFLUENCE<<<<<<
>>>>>AND COMPUTE VARIOUS CONFLUENCED STREAM VALUES<<<<<<

=====

TOTAL NUMBER OF STREAMS = 2
CONFLUENCE VALUES USED FOR INDEPENDENT STREAM 2 ARE:
TIME OF CONCENTRATION(MIN.) = 10.99
RAINFALL INTENSITY(INCH/HR) = 1.44
AREA-AVERAGED Fm(INCH/HR) = 0.26
AREA-AVERAGED Fp(INCH/HR) = 0.26
AREA-AVERAGED Ap = 1.00
EFFECTIVE STREAM AREA(ACRES) = 2.36
TOTAL STREAM AREA(ACRES) = 2.36
PEAK FLOW RATE(CFS) AT CONFLUENCE = 2.61

** CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	24.47	18.62	1.064	0.27(0.27)	1.00	34.2	10.00
2	2.61	10.99	1.440	0.26(0.26)	1.00	2.4	31.00

RAINFALL INTENSITY AND TIME OF CONCENTRATION RATIO
CONFLUENCE FORMULA USED FOR 2 STREAMS.

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	23.90	10.99	1.440	0.27(0.27)	1.00	22.6	31.00
2	26.26	18.62	1.064	0.27(0.27)	1.00	36.6	10.00

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE(CFS) = 26.26 Tc(MIN.) = 18.62
EFFECTIVE AREA(ACRES) = 36.57 AREA-AVERAGED Fm(INCH/HR) = 0.27
AREA-AVERAGED Fp(INCH/HR) = 0.27 AREA-AVERAGED Ap = 1.00
TOTAL AREA(ACRES) = 36.6

LONGEST FLOWPATH FROM NODE 10.00 TO NODE 14.00 = 1942.00 FEET.

FLOW PROCESS FROM NODE 14.00 TO NODE 15.00 IS CODE = 31

>>>>>COMPUTE PIPE-FLOW TRAVEL TIME THRU SUBAREA<<<<<<
>>>>>USING COMPUTER-ESTIMATED PIPESIZE (NON-PRESSURE FLOW)<<<<<<

=====

ELEVATION DATA: UPSTREAM(FEET) = 596.00 DOWNSTREAM(FEET) = 590.00
FLOW LENGTH(FEET) = 82.00 MANNING'S N = 0.013
DEPTH OF FLOW IN 21.0 INCH PIPE IS 12.5 INCHES
PIPE-FLOW VELOCITY(FEET/SEC.) = 17.58
ESTIMATED PIPE DIAMETER(INCH) = 21.00 NUMBER OF PIPES = 1
PIPE-FLOW(CFS) = 26.26
PIPE TRAVEL TIME(MIN.) = 0.08 Tc(MIN.) = 18.69
LONGEST FLOWPATH FROM NODE 10.00 TO NODE 15.00 = 2024.00 FEET.

FLOW PROCESS FROM NODE 15.00 TO NODE 16.00 IS CODE = 91

>>>>>COMPUTE "V" GUTTER FLOW TRAVEL TIME THRU SUBAREA<<<<<

=====

UPSTREAM NODE ELEVATION(FEET) = 590.00
DOWNSTREAM NODE ELEVATION(FEET) = 578.00
CHANNEL LENGTH THRU SUBAREA(FEET) = 29.00
"V" GUTTER WIDTH(FEET) = 5.00 GUTTER HIKE(FEET) = 0.050
PAVEMENT LIP(FEET) = 0.010 MANNING'S N = .0500
PAVEMENT CROSSFALL(DECIMAL NOTATION) = 0.00200
MAXIMUM DEPTH(FEET) = 3.00
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.057
SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL GOOD COVER					
"WOODLAND"	B	0.01	0.30	1.000	55

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30
SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 26.26
TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.23
AVERAGE FLOW DEPTH(FEET) = 0.18 FLOOD WIDTH(FEET) = 126.30
"V" GUTTER FLOW TRAVEL TIME(MIN.) = 0.15 Tc(MIN.) = 18.84
SUBAREA AREA(ACRES) = 0.01 SUBAREA RUNOFF(CFS) = 0.01
EFFECTIVE AREA(ACRES) = 36.58 AREA-AVERAGED Fm(INCH/HR) = 0.27
AREA-AVERAGED Fp(INCH/HR) = 0.27 AREA-AVERAGED Ap = 1.00
TOTAL AREA(ACRES) = 36.6 PEAK FLOW RATE(CFS) = 26.26
NOTE: PEAK FLOW RATE DEFAULTED TO UPSTREAM VALUE

END OF SUBAREA "V" GUTTER HYDRAULICS:

DEPTH(FEET) = 0.18 FLOOD WIDTH(FEET) = 126.30
FLOW VELOCITY(FEET/SEC.) = 3.23 DEPTH*VELOCITY(FT*FT/SEC) = 0.58
LONGEST FLOWPATH FROM NODE 10.00 TO NODE 16.00 = 2053.00 FEET.

FLOW PROCESS FROM NODE 16.00 TO NODE 16.00 IS CODE = 10

>>>>>MAIN-STREAM MEMORY COPIED ONTO MEMORY BANK # 1 <<<<<

FLOW PROCESS FROM NODE 50.00 TO NODE 51.00 IS CODE = 21

>>>>>RATIONAL METHOD INITIAL SUBAREA ANALYSIS<<<<<
>>USE TIME-OF-CONCENTRATION NOMOGRAPH FOR INITIAL SUBAREA<<

=====

INITIAL SUBAREA FLOW-LENGTH(FEET) = 297.00
ELEVATION DATA: UPSTREAM(FEET) = 698.30 DOWNSTREAM(FEET) = 693.50

Tc = K*[(LENGTH** 3.00)/(ELEVATION CHANGE)]**0.20
SUBAREA ANALYSIS USED MINIMUM Tc(MIN.) = 11.683
* 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.391
SUBAREA Tc AND LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN	Tc (MIN.)
NATURAL POOR COVER						
"GRASS"	C	0.30	0.25	1.000	86	11.68

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.25
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 1.000
 SUBAREA RUNOFF (CFS) = 0.31
 TOTAL AREA (ACRES) = 0.30 PEAK FLOW RATE (CFS) = 0.31

 FLOW PROCESS FROM NODE 51.00 TO NODE 52.00 IS CODE = 91

>>>>COMPUTE "V" GUTTER FLOW TRAVEL TIME THRU SUBAREA<<<<<

=====

UPSTREAM NODE ELEVATION (FEET) = 693.50
 DOWNSTREAM NODE ELEVATION (FEET) = 666.50
 CHANNEL LENGTH THRU SUBAREA (FEET) = 1046.00
 "V" GUTTER WIDTH (FEET) = 5.00 GUTTER HIKE (FEET) = 0.050
 PAVEMENT LIP (FEET) = 0.010 MANNING'S N = .0150
 PAVEMENT CROSSFALL (DECIMAL NOTATION) = 0.20000
 MAXIMUM DEPTH (FEET) = 3.00
 * 2 YEAR RAINFALL INTENSITY (INCH/HR) = 1.095
 SUBAREA LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN
NATURAL POOR COVER "GRASS"	C	2.50	0.25	1.000	86

SUBAREA AVERAGE PERVIOUS LOSS RATE, F_p (INCH/HR) = 0.25
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, A_p = 1.000
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW (CFS) = 1.16
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY (FEET/SEC.) = 2.89
 AVERAGE FLOW DEPTH (FEET) = 0.10 FLOOD WIDTH (FEET) = 5.44
 "V" GUTTER FLOW TRAVEL TIME (MIN.) = 6.04 T_c (MIN.) = 17.72
 SUBAREA AREA (ACRES) = 2.50 SUBAREA RUNOFF (CFS) = 1.90
 EFFECTIVE AREA (ACRES) = 2.80 AREA-AVERAGED F_m (INCH/HR) = 0.25
 AREA-AVERAGED F_p (INCH/HR) = 0.25 AREA-AVERAGED A_p = 1.00
 TOTAL AREA (ACRES) = 2.8 PEAK FLOW RATE (CFS) = 2.13

END OF SUBAREA "V" GUTTER HYDRAULICS:

DEPTH (FEET) = 0.14 FLOOD WIDTH (FEET) = 5.77
 FLOW VELOCITY (FEET/SEC.) = 3.62 DEPTH*VELOCITY (FT*FT/SEC) = 0.49
 LONGEST FLOWPATH FROM NODE 50.00 TO NODE 52.00 = 1343.00 FEET.

 FLOW PROCESS FROM NODE 52.00 TO NODE 53.00 IS CODE = 91

>>>>COMPUTE "V" GUTTER FLOW TRAVEL TIME THRU SUBAREA<<<<<

=====

UPSTREAM NODE ELEVATION (FEET) = 666.50
 DOWNSTREAM NODE ELEVATION (FEET) = 606.00
 CHANNEL LENGTH THRU SUBAREA (FEET) = 397.00
 "V" GUTTER WIDTH (FEET) = 5.00 GUTTER HIKE (FEET) = 0.050
 PAVEMENT LIP (FEET) = 0.010 MANNING'S N = .0150
 PAVEMENT CROSSFALL (DECIMAL NOTATION) = 0.20000
 MAXIMUM DEPTH (FEET) = 3.00
 * 2 YEAR RAINFALL INTENSITY (INCH/HR) = 1.064
 SUBAREA LOSS RATE DATA (AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	F_p (INCH/HR)	A_p (DECIMAL)	SCS CN
NATURAL POOR COVER "GRASS"	A	0.03	0.40	1.000	67

NATURAL POOR COVER
 "GRASS" B 1.53 0.30 1.000 78
 NATURAL POOR COVER
 "GRASS" C 1.16 0.25 1.000 86
 NATURAL POOR COVER
 "GRASS" D 0.08 0.20 1.000 89
 SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.28
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 3.12
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 7.31
 AVERAGE FLOW DEPTH(FEET) = 0.11 FLOOD WIDTH(FEET) = 5.48
 "V" GUTTER FLOW TRAVEL TIME(MIN.) = 0.91 Tc(MIN.) = 18.63
 SUBAREA AREA(ACRES) = 2.80 SUBAREA RUNOFF(CFS) = 1.98
 EFFECTIVE AREA(ACRES) = 5.60 AREA-AVERAGED Fm(INCH/HR) = 0.26
 AREA-AVERAGED Fp(INCH/HR) = 0.26 AREA-AVERAGED Ap = 1.00
 TOTAL AREA(ACRES) = 5.6 PEAK FLOW RATE(CFS) = 4.03

END OF SUBAREA "V" GUTTER HYDRAULICS:
 DEPTH(FEET) = 0.12 FLOOD WIDTH(FEET) = 5.62
 FLOW VELOCITY(FEET/SEC.) = 7.96 DEPTH*VELOCITY(FT*FT/SEC) = 0.97
 LONGEST FLOWPATH FROM NODE 50.00 TO NODE 53.00 = 1740.00 FEET.

FLOW PROCESS FROM NODE 53.00 TO NODE 16.00 IS CODE = 91

>>>>COMPUTE "V" GUTTER FLOW TRAVEL TIME THRU SUBAREA<<<<<

=====

UPSTREAM NODE ELEVATION(FEET) = 606.00
 DOWNSTREAM NODE ELEVATION(FEET) = 578.00
 CHANNEL LENGTH THRU SUBAREA(FEET) = 398.00
 "V" GUTTER WIDTH(FEET) = 5.00 GUTTER HIKE(FEET) = 0.050
 PAVEMENT LIP(FEET) = 0.010 MANNING'S N = .0500
 PAVEMENT CROSSFALL(DECIMAL NOTATION) = 0.20000
 MAXIMUM DEPTH(FEET) = 3.00
 * 2 YEAR RAINFALL INTENSITY(INCH/HR) = 1.000
 SUBAREA LOSS RATE DATA(AMC II):

DEVELOPMENT TYPE/ LAND USE	SCS SOIL GROUP	AREA (ACRES)	Fp (INCH/HR)	Ap (DECIMAL)	SCS CN
NATURAL GOOD COVER "WOODLAND"	A	0.65	0.40	1.000	25
NATURAL GOOD COVER "WOODLAND"	B	2.13	0.30	1.000	55
NATURAL GOOD COVER "WOODLAND"	C	1.04	0.25	1.000	70

SUBAREA AVERAGE PERVIOUS LOSS RATE, Fp(INCH/HR) = 0.30
 SUBAREA AVERAGE PERVIOUS AREA FRACTION, Ap = 1.000
 TRAVEL TIME COMPUTED USING ESTIMATED FLOW(CFS) = 5.23
 TRAVEL TIME THRU SUBAREA BASED ON VELOCITY(FEET/SEC.) = 3.10
 AVERAGE FLOW DEPTH(FEET) = 0.30 FLOOD WIDTH(FEET) = 7.43
 "V" GUTTER FLOW TRAVEL TIME(MIN.) = 2.14 Tc(MIN.) = 20.77
 SUBAREA AREA(ACRES) = 3.82 SUBAREA RUNOFF(CFS) = 2.39
 EFFECTIVE AREA(ACRES) = 9.42 AREA-AVERAGED Fm(INCH/HR) = 0.28
 AREA-AVERAGED Fp(INCH/HR) = 0.28 AREA-AVERAGED Ap = 1.00
 TOTAL AREA(ACRES) = 9.4 PEAK FLOW RATE(CFS) = 6.10

END OF SUBAREA "V" GUTTER HYDRAULICS:
 DEPTH(FEET) = 0.33 FLOOD WIDTH(FEET) = 7.68

FLOW VELOCITY (FEET/SEC.) = 3.26 DEPTH*VELOCITY (FT*FT/SEC) = 1.07
LONGEST FLOWPATH FROM NODE 50.00 TO NODE 16.00 = 2138.00 FEET.

FLOW PROCESS FROM NODE 16.00 TO NODE 16.00 IS CODE = 11

>>>>CONFLUENCE MEMORY BANK # 1 WITH THE MAIN-STREAM MEMORY<<<<<

** MAIN STREAM CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	6.10	20.77	1.000	0.28 (0.28)	1.00	9.4	50.00
LONGEST FLOWPATH FROM NODE 50.00 TO NODE 16.00 =					2138.00 FEET.		

** MEMORY BANK # 1 CONFLUENCE DATA **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	23.90	11.23	1.423	0.27 (0.27)	1.00	22.6	31.00
2	26.26	18.84	1.057	0.27 (0.27)	1.00	36.6	10.00
LONGEST FLOWPATH FROM NODE 10.00 TO NODE 16.00 =					2053.00 FEET.		

** PEAK FLOW RATE TABLE **

STREAM NUMBER	Q (CFS)	Tc (MIN.)	Intensity (INCH/HR)	Fp(Fm) (INCH/HR)	Ap	Ae (ACRES)	HEADWATER NODE
1	29.14	11.23	1.423	0.27 (0.27)	1.00	27.7	31.00
2	32.23	18.84	1.057	0.27 (0.27)	1.00	45.1	10.00
3	30.45	20.77	1.000	0.27 (0.27)	1.00	46.0	50.00
TOTAL AREA (ACRES) =					46.0		

COMPUTED CONFLUENCE ESTIMATES ARE AS FOLLOWS:

PEAK FLOW RATE (CFS) = 32.23 Tc (MIN.) = 18.844
EFFECTIVE AREA (ACRES) = 45.13 AREA-AVERAGED Fm (INCH/HR) = 0.27
AREA-AVERAGED Fp (INCH/HR) = 0.27 AREA-AVERAGED Ap = 1.00
TOTAL AREA (ACRES) = 46.0
LONGEST FLOWPATH FROM NODE 50.00 TO NODE 16.00 = 2138.00 FEET.

FLOW PROCESS FROM NODE 16.00 TO NODE 16.00 IS CODE = 12

>>>>CLEAR MEMORY BANK # 1 <<<<<

FLOW PROCESS FROM NODE 16.00 TO NODE 17.00 IS CODE = 91

>>>>COMPUTE "V" GUTTER FLOW TRAVEL TIME THRU SUBAREA<<<<<

UPSTREAM NODE ELEVATION (FEET) = 578.00
DOWNSTREAM NODE ELEVATION (FEET) = 558.83
CHANNEL LENGTH THRU SUBAREA (FEET) = 466.00
"V" GUTTER WIDTH (FEET) = 5.00 GUTTER HIKE (FEET) = 0.050
PAVEMENT LIP (FEET) = 0.010 MANNING'S N = .0500
PAVEMENT CROSSFALL (DECIMAL NOTATION) = 0.20000
MAXIMUM DEPTH (FEET) = 6.00
* 2 YEAR RAINFALL INTENSITY (INCH/HR) = 1.004
SUBAREA LOSS RATE DATA (AMC II):